



# **Life Cycle Assessment of Polymers in an Automotive Bolster**

for  
American Chemistry Council

by  
PE INTERNATIONAL, Inc.

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## ABBREVIATIONS

ACC	American Chemistry Council
CML	Centre of Environmental Science at Leiden
CO <sub>2</sub>	Carbon dioxide
DE	Germany dataset country code
EoL	End-of-Life
EPA	Environmental Protection Agency
GaBi	Ganzheitliche Bilanzierung (German for holistic balancing). The GaBi 4 software for life cycle engineering, developed by PE INTERNATIONAL AG, is a market-leading software package for LCA modeling. PE INTERNATIONAL's GaBi database contains life cycle inventory data.
GHG	Greenhouse gas
GLO	Global dataset country code
GWP	Global Warming Potential
H <sup>+</sup>	Hydron (hydrogen cation)
IPCC	Intergovernmental Panel on Climate Change
ISO	International Organization for Standardization
LCA	Life Cycle Assessment
LCI	Life Cycle Inventory
LCIA	Life Cycle Impact Assessment
MJ	Megajoule
N	Nitrogen
NO <sub>x</sub>	Nitrogen oxides
NREL	National Renewable Energy Laboratory, Golden, CO
P	Phosphorous
PED	Primary Energy Demand
POCP	Photochemical Ozone Creation Potential
RNA	North America dataset country code
TRACI	US EPA's Tool for the Reduction and Assessment of Chemical and Other Environmental Impacts
US	United States dataset country code
VOC	Volatile Organic Compound

## 1 EXECUTIVE SUMMARY

This life cycle assessment study carried out on behalf of the American Chemistry Council (ACC) assesses the life cycle performance of polymers in comparison to metals for an automotive bolster. ACC plans on using this case study to:

- Understand the potential life cycle impact of using polymers in an automotive application where metals are more commonly used
- Encourage the use of life cycle thinking in the choice of materials when designing auto parts
- Identify whether the use of polymers shows environmental benefits in this application
- Inform design for environment efforts in the automotive industry with quantitative potential life cycle impact information.

The cradle-to-grave LCA considers a total service life of 150,000 miles for a Ford Taurus 2008 metal and plastic bolster (baseline product) compared to the 2005 metal and plastic bolster and the 2010 plastic bolster. The 2005 bolster is 14% lighter than the 2008 bolster. The 2010 bolster is 46% lighter than the 2008 bolster.

This report describes the environmental impacts by life cycle stage, as well as the total difference in impact of each comparison product to the baseline product. The life cycle stages included in this LCA study address the production of upstream materials and energy, product manufacturing, use, and the end-of-life treatment for all materials used throughout the life cycle. The report and the underlying methodologies and approaches have undergone external, independent critical review and fully comply with the requirements of the ISO 14040/14044 standards. The inventory and impact categories assessed are non-renewable primary energy demand, global warming potential, acidification potential, eutrophication potential, and smog potential. For detailed descriptions see Appendix A: Life Cycle Impact Assessment Categories.

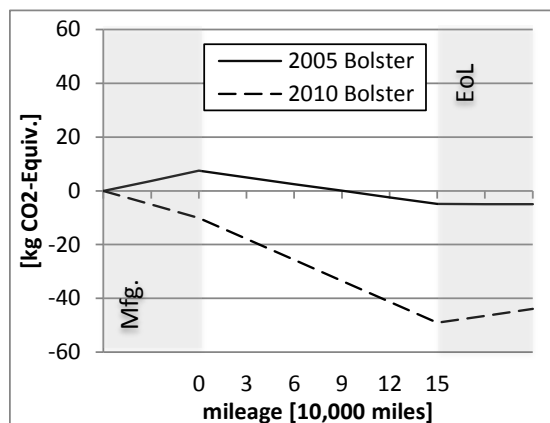
The results, as exemplified by the figure below for global warming potential, show that the lightweight product outperforms the metal product, meaning that the net impact indicator over the full life cycle is lower. This is expressed by a net negative value, since the performance is shown as the difference from the baseline (alternative product results minus baseline metal product results).

Applying US EPA's TRACI normalization factors<sup>1</sup> also demonstrated that summer smog and eutrophication potential only make minor contributions to the environmental profile compared to the other impact categories in this study. Therefore, the table below only shows primary energy demand, global warming potential, and acidification potential.

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<sup>1</sup> Bare et al: Development of the Method and U.S. Normalization Database for Life Cycle Impact Assessment and Sustainability Metrics, Environmental Science & Technology (2006) 40:5108-5115





**Bolster Global Warming Potential –  
Alternative Minus Baseline**

Alternative Minus Baseline	Primary Energy Demand (net calorific value) [MJ]		Global Warming Potential (100 years) [kg CO2-Equiv.]		Acidification Potential [mol H+ Equiv.]	
	No Drive Train Adaptation	With Drive Train Adaptation	No Drive Train Adaptation	With Drive Train Adaptation	No Drive Train Adaptation	With Drive Train Adaptation
2005 Bolster	-87.63	-316.29	-4.99	-21.89	-1.76	-2.48
2010 Bolster	-605.52	-1328.96	-43.87	-97.34	-2.37	-4.67

When comparing to the baseline product, the following results were found (see also table):

- The lighter-than-baseline 2005 bolster and 2010 bolster perform better than the baseline 2008 bolster for global warming potential, primary energy demand, and acidification potential.
- The 2010 bolster is also lighter than and performs better than the 2005 bolster in all considered impact categories.

An even greater benefit is possible if additional parts on the vehicle are also reduced in mass to an extent that allows for adaptations to the drive train or gearbox (reduction of engine displacement or elongation of gear ratio) while maintaining constant vehicle performance. These measures allow the use phase savings to be more than doubled.<sup>2</sup> Since the extent of additional lightweight measures was unknown in this project, the drive train adaptation was considered as a potential scenario only. To harvest the benefits of lightweighting to their full extent, it is recommended that the sum of all mass reductions in the design process should be monitored and, whenever feasible, invested into fuel economy by adapting the drive train while maintaining constant vehicle performance. This scenario will become increasingly likely in the future since the Corporate Average Fuel Economy (CAFE) standards for model years 2012-2016 passenger cars and light trucks requires an estimated combined average mile per gallon level of 34.1 by model year 2016.

<sup>2</sup> See Section 4.2 Calculation of Use Phase Fuel Savings, which refers to Koffler & Rohde-Brandenburger: On the calculation of fuel savings through lightweight design in automotive life cycle assessments, Int J Life Cycle Assess (2010) 15:128-135

The potential benefit of plastic parts would also increase if the US adopts end-of-life regulations, such as in Europe, for re-use and recovery of vehicle parts rather than disposal to landfill, since this study assumes that all plastic goes to landfill at end-of-life based on current conditions.

Concluding, it appears reasonable to state that while the lighter products show only small differences to the 2008 bolster with regard to summer smog and eutrophication, they have the potential to lower the global warming potential, primary energy demand, and acidification potential of their metal counterpart over the full life cycle. Future conditions such as more stringent fuel economy and end-of-life regulations will likely increase this potential benefit across all impact categories. These conclusions are drawn for the specific parts examined in this study and shall not be generalized to encompass all plastic vs. metal part comparisons. Specific design options should always be assessed on a case-by-case basis whether for environmental, cost, or performance purposes as different materials or combinations of materials may render different results.

## 2 GOAL OF THE STUDY

The comparative life cycle assessment (LCA) project outlined in this document was carried out on behalf of the American Chemistry Council (ACC), and considers the potential life cycle environmental impacts of using polymers as an alternative to metals in the design of an automotive bolster. ACC plans on using this case study to:

- Understand the potential life cycle impact potential of using polymers in an automotive application
- Encourage the use of life cycle thinking in the choice of materials when designing auto parts
- Identify whether the use of polymers shows environmental benefits in this application
- Inform design for environment efforts in the automotive industry with quantitative potential life cycle impact information.

The goal of this study is to assess the life cycle environmental performance of engineering polymers in comparison to metals which are more commonly used in the considered automotive applications. A general review of the relative performance attributes and potential life cycle impacts / benefits of these materials were considered, as well as detailed examination of the case study in which polymers were used to replace metal parts in a high-volume automotive application.

This study provides ACC with a quantitative point of reference of the environmental life cycle performance of polymer use in automotive applications, and will aid product development and decision-making amongst member companies and stakeholders. This study is intended to be an ISO 14040-series compliant life cycle assessment (LCA).

Potential stakeholders for this project include:

- The ACC automotive group
- The ACC member companies
- Automotive designers and manufacturers
- Automotive supply chain managers
- Automotive part suppliers
- Polymer manufacturers

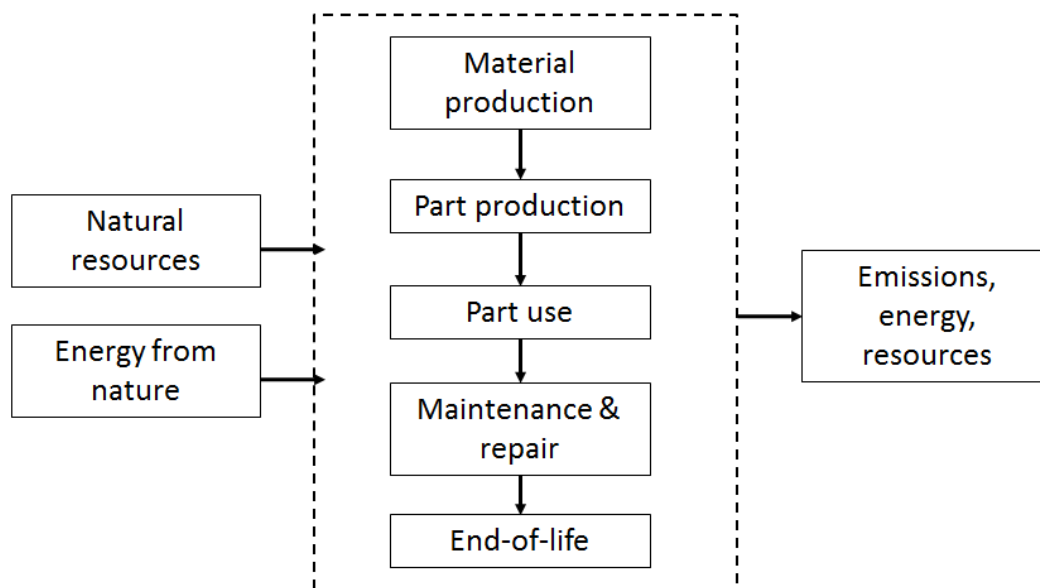
The results of this comparative study were critically reviewed for communication and distribution to external stakeholders.

### 3 SCOPE OF THE STUDY

The following section describes the general scope of the project to achieve the stated goals. This includes the identification of specific products assessed, the supporting product systems, the system boundary, allocation procedures, and cut-off criteria. See Chapter 4 for a detailed description of data collection, modeling assumptions, and background data.

#### 3.1 SYSTEM DESCRIPTION

The life cycle stages for the system being considered are shown in Figure 1. This study assesses the full life cycle – from cradle to grave – of the conventional and polymer part designs being considered. The system boundaries are consistent between all models.



**Figure 1: Life Cycle Flow Diagram for System of Study**

Material production refers to the extraction and preparation of the materials used. Part production refers to the manufacture of materials into vehicle parts. The use phase includes the impact potential associated with all fuel savings (combustion and upstream production) caused by the lower weight of the plastic parts during the vehicle's lifetime, as well as any parts or consumables expected to be required for the upkeep, maintenance, or repair of the part during the vehicle's lifetime. The products' end-of-life includes a mix of landfilling and recycling.

#### 3.2 FUNCTIONAL UNIT

This case study examines the evolution of the Ford Taurus bolster, from different plastic and steel assemblies in 2005 and 2008, to a one-piece direct long fiber thermoplastic polypropylene (DLFT) bolster with glass reinforcement for the hood latch in 2010. Because the 2008 bolster is actually the heaviest of the three bolsters, it is set as the baseline for the comparison of results.

The services provided by a bolster are manifold. Some of the main requirements are that it has to endure hood slams and hood latch pulls, provide support for the attachment of the radiator, resist fatigue due to vibration, and display certain behaviors in a crash. The functional unit is chosen to be “providing structural and component support of a vehicle front over a vehicle lifetime of 150,000 miles.” The common level of quality is passing the Ford latch pull test to support a load of 5,340N without separation because this is considered the most significant structural requirement.

A service life of 150,000 miles is selected as an estimate of vehicle design life, and is not intended to represent the actual average lifetime of the vehicle. It expresses the authors’ belief that lightweight measures should break-even within a reasonable mileage and is less than the typical lifetime mileage of 152,137 miles for passenger cars and 179,954 miles for light trucks.<sup>3</sup>

Maintenance is excluded as a bolster does not require general maintenance.

### 3.3 STUDY BOUNDARIES

This study assesses the complete life cycle of the functional unit as shown in Figure 1 and described in Section 3.2. This includes all of the relevant upstream production of materials and energies, part production, use, and end-of-life disposition. A summary of what is included and excluded in this study is shown in Table 1.

**Table 1: System Boundaries**

Included	Excluded
✓ Upstream raw material production	✗ Capital equipment and maintenance
✓ Upstream energy production	✗ Overhead (heating, lighting) of manufacturing facilities if separable
✓ Mechanical part production	✗ Part assembly
✓ Transportation of all materials up to the assembly point and finished product distribution to regional distribution sites	✗ In-plant transportation
✓ Use	✗ Human labor
✓ Service (repair and replacement)	
✓ End-of-life disposition	
✓ Transportation of raw materials, finished product and parts, as required for service activities	

#### 3.3.1 Technology Coverage

Design data for the part production at the time of the technology changeover were collected and analyzed wherever possible. For all upstream parts and materials, average industry profiles from the GaBi 4 databases were utilized.

#### 3.3.2 Geographic Coverage

The geographic region considered is limited to the North American auto market, with focus on the US. Accordingly, data were chosen to be representative for the US or North American markets whenever possible. For datasets used including geographic coverage, see Section 4.1.4.

<sup>3</sup> U.S. Department of Transportation, National Highway Traffic Safety Administration, Vehicle Survivability and Travel Mileage Schedules, January 2006.

### 3.3.3 Time Coverage

Design data is based on production at the time of changeover from metal to plastic parts. Additional data necessary to model material production and energy use were obtained from the GaBi Databases 2006 and are representative of years 2002 to present. For datasets used including reference years, see Section 4.1.4.

## 3.4 SELECTION OF IMPACT ASSESSMENT CATEGORIES

The following inventory flows and environmental categories considered to be of high relevance to the goals of the project were investigated:

- Non-renewable Primary Energy Demand
- Global Warming Potential
- Acidification Potential
- Eutrophication Potential
- Smog Potential

For detailed descriptions, see Appendix A: Life Cycle Impact Assessment Categories.

For the purposes of this project, it is expected that results will be primarily used in the USA, and so the TRACI impact categorization methodology<sup>4</sup> has been used for Eutrophication, Acidification, and Smog. A recent update of the IPCC factors for climate change<sup>5</sup> is not reflected in the TRACI characterization factors, so CML factors<sup>6</sup> (which were updated with IPCC data in November 2009) have been used to evaluate Global Warming Potential.

In addition to the environmental impact categories noted above, the study includes an evaluation of human toxicity and ecotoxicity using the USEtox characterization model. The precision of the current USEtox characterization factors is within a factor of 100–1,000 for human health and 10–100 for freshwater ecotoxicity.<sup>7</sup> This is a substantial improvement over previously available toxicity characterization models, but still higher than for the other impacts noted above.

Therefore, the USEtox characterization factors are used within this study to identify key contributors within product life cycles which influence that product's toxicity potential. The life cycle results would indicate which materials show up as substances of high concern, but shall not be used to make any comparative assertions.

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<sup>4</sup> Bare et al., TRACI: the Tool for the Reduction and Assessment of Chemical and Other Environmental Impacts JIE, MIT Press, 2002.

<sup>5</sup> Intergovernmental Panel on Climate Change (IPCC). Climate Change 2007: The Physical Science Basis. Contribution of Working Group I to the Fourth Assessment. Report of the Intergovernmental Panel on Climate Change. 2007.

<sup>6</sup> <http://cml.leiden.edu/software/data-cmlia.html>

<sup>7</sup> Rosenbaum et al (2008): USEtox—the UNEP-SETAC toxicity model: recommended characterisation factors for human toxicity and freshwater ecotoxicity in life cycle impact assessment, Int J Life Cycle Assess (2008) 13:532–546

### 3.5 DATA COLLECTION

Supply of primary data on the design of the parts, including the bill of materials and types of processes employed for part production, were coordinated by ACC through contacts with the auto and auto part manufacturers. No site-specific manufacturing inventory data (e.g., energy consumption and emissions) were collected.

Data for energy consumption during the use phase were calculated, as described in Section 4.2.

In addition to primary process data, each model utilized GaBi background data (i.e., for upstream raw materials and energies, part production, transportation, and end-of-life).

#### 3.5.1 Fuels and Energy

Average fuels and energy inputs were obtained from the GaBi 4 Software database. See Section 4.1.4 for datasets used.

#### 3.5.2 Raw and Process Materials

Inventory data for all upstream raw materials and mechanical components were obtained from the GaBi 4 Software database. USLCI data for plastics<sup>8</sup> and worldsteel data for steel were utilized when available; otherwise PE data were used. See Section 4.1.4 for datasets used.

#### 3.5.3 Co-product and By-product Allocation

No allocation was necessary to co- or by-products in the current scope of the study besides the allocation inherent to the upstream datasets (e.g., allocation between refinery products).

#### 3.5.4 End-of-Life Disposition

The products' end-of-life includes a mix of landfilling and recycling. Recycling of manufacturing scrap and at end-of-life was modeled using the "avoided burden" approach, giving credits for potential material recovery. See Section 4.1.4 and Section 4.3 for more details. Alternatively, results using the "cut-off" approach are provided in Section 6.3.

#### 3.5.5 Cut-off Criteria

The cut-off criteria for the study include or exclude materials, energy and emissions data as follows:

- Mass – If a flow is less than 2% of the cumulative mass of the intermediate input flows of the model it may be excluded, providing its environmental relevance is not a concern.
- Energy – If a flow is less than 2% of the cumulative energy of the intermediate input flows of the model it may be excluded, providing its environmental relevance is not a concern.
- Environmental relevance – If a flow meets the above criteria for exclusion, yet is thought to potentially have a significant environmental impact, it is included. Elementary output flows (emissions) which have an environmental impact that is greater than 2% of the whole impact of

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<sup>8</sup> Data in the USLCI database were critically reviewed according to the USLCI data review protocol; see <http://www.nrel.gov/lci/database/>. Results using plastics data from USLCI were compared with results using other plastics data sources.

an impact category that has been considered in the assessment must be covered. This judgment was done based on experience and documented as necessary.

### **3.5.6 Data Quality**

Under the guidance of PE INTERNATIONAL, ACC technical experts and personnel collected the data for the processes associated with production, service, use, and logistics. PE INTERNATIONAL gathered the remaining data representative of the full product system utilizing the GaBi database in its current version. This modeling approach ensures that all materials are modeled according to the same boundary conditions, the analysis does not compare different background systems, and that the results represent current technology and up to date background data.

Chapter 4 describes the primary and background data utilized in the life cycle model as well as any assumptions.

Auto part production was modeled based on:

- Primary data for the material composition (measured), scrap generation (calculated), and which type of manufacturing processes are used (e.g., stamping, deep drawing).
- GaBi upstream data

Use phase was modeled based on:

- Calculated reduction of fuel consumption and CO<sub>2</sub> and SO<sub>2</sub> emissions from lightweight design
- GaBi upstream data

End-of-life disposition was modeled based on:

- End-of-life scenarios (e.g., percent to landfill)
- GaBi upstream data

Because the model is based on direct measurement of the product design, the data quality is expected to be high.

### **3.5.7 Exceptions**

There were no exceptions to the aforementioned data collection scope.

## **3.6 SOFTWARE AND DATABASE**

The LCA model was created using the GaBi 4 Software system for life cycle engineering, developed by PE INTERNATIONAL AG. The GaBi database provides the life cycle inventory data for several of the raw and process materials obtained from the background system.

## **3.7 INTERPRETATION**

The results of the LCI/LCIA are interpreted according to the Goal and Scope. The interpretation addresses the following topics:



- Identification of significant findings, such as the main materials contributing to the overall results, the contribution of the main energy carriers used in the process and the potential contribution of emissions for main impact categories in the context of the whole life cycle.
- Evaluation of completeness, sensitivity and consistency, to justify the inclusion or exclusion of data from the system boundaries as well as the cut-off criteria and data quality checks.
- Conclusions, limitations and recommendations, should state the appropriateness of the definitions of the system functions, the functional unit and system boundary.

### 3.8 CRITICAL REVIEW

Because the study is comparative and is intended to support external communications, a critical review was conducted. The critical review panel consisted of the following members:

- Dr. Roland Geyer, Associate Professor, Bren School of Environmental Science & Management, University of California, Santa Barbara (Chair)
- Dr. Allan Murray, President, Ecoplexus Inc., and CTO, Allied Composite Technologies LLC
- Dr. John L. Sullivan, Sustainable Development Strategies, LLC

The critical review process was completed in three stages:

- Stage 1: Review of the Study Purpose, Boundaries, and Data Categories
  - Ensure purpose and goal of study is clearly defined
  - Ensure that all necessary data categories (inventory and impact) are covered to meet goal
  - Understand how results will be used
  - Ensure that the study meets quality requirements
- Stage 2: Mid-project review at point of LCI completion
  - Ensure recommendations of Stage 1 were addressed
  - Verify adequacy of data collection and model
  - Ensure that data quality meets quality requirements
- Stage 3: Review of the Draft Final Report
  - Ensure feedback of Stage 2 was addressed
  - Confirm that the observations and conclusions from the study are consistent with the stated purpose
  - Ensure overall study quality and how the study meets the data quality specifications that are relevant to the stated purpose

After incorporation of the Review Panel's comments into the final report, the Chair of the panel issued a Critical Review Report. A copy can be found in Appendix B: Critical Review Report.

### **3.9 QUALITY ASSURANCE**

In addition to the full ISO-compliant critical review conducted over the course of the study, an internal quality assurance review was performed by PE INTERNATIONAL in-house experts that have not conducted the analytical work contained within this study.

### **3.10 DELIVERABLES**

This project results in an ISO 14040/14044 compliant report describing the potential life cycle environmental impacts associated with a case study in which polymer parts replaced metal parts with the same function.

This report was critically reviewed, and the final report integrates feedback from the reviewers as well as reviewer comments. This critically reviewed report is appropriate for both internal and external communication.

## 4 LIFE CYCLE INVENTORY

This chapter describes the LCI datasets and gate-to-gate processes used to model each life cycle step.

### 4.1 CRADLE-TO-GATE PRODUCTION

Sections 4.1.1 to 4.1.3 provide the material composition for each product and the inputs required (includes scrap generation) as provided by ACC through its contacts in the auto industry. The material composition was measured and the scrap generation was calculated. Section 4.1.4 describes the modeling of part production including the background material and energy datasets used and the manufacturing of materials into parts.

#### 4.1.1 2008 Ford Taurus Front End Bolster Material Composition (Baseline)

Table 2 provides the material composition of the 7.597 kg Ford front end bolster. The difference between the input materials and the finished part is the production scrap, which is sent to a recycler.

**Table 2: 2008 Bolster Material Composition**

Material	Input [kg]	Finished Part [kg]	Finished Part [%]
Plastic support	4.096	3.960	52%
<i>Polypropylene</i>	2.458	2.376	60%
<i>Glass fiber</i>	1.638	1.584	40%
Steel e-coated bracket reinforcements (2)	4.365	2.104	28%
Steel e-coated boomerang reinforcement	3.304	1.333	18%
Steel fasteners	0.200	0.200	3%
<b>Total</b>	<b>11.965</b>	<b>7.597</b>	<b>100%</b>

#### 4.1.2 2005 Ford Taurus Front End Bolster Material Composition

Table 3 provides the material composition of the 6.496 kg Ford front end bolster. The difference between the input materials and the finished part is the production scrap, which is sent to a recycler.

**Table 3: 2005 Bolster Material Composition**

Material	Input [kg]	Finished Part [kg]	Finished Part [%]
Plastic support	2.821	2.752	42.4%
<i>Nylon 6</i>	1.975	1.926	70%
<i>Glass fiber</i>	0.846	0.826	30%
Steel e-coated crossmember + 2 extensions	5.703	3.106	47.8%
Steel e-coated latch mounting	0.875	0.568	8.7%
Brass fasteners	0.024	0.024	0.4%
Aluminum fasteners	0.006	0.006	0.1%
Steel fasteners	0.040	0.040	0.6%
<b>Total</b>	<b>9.469</b>	<b>6.496</b>	<b>100%</b>

#### 4.1.3 2010 Ford Taurus Front End Bolster Material Composition

Table 4 provides the material composition of the 4.114 kg Ford front end bolster. The difference between the input materials and the finished part is the production scrap, which is sent to a recycler.

**Table 4: 2010 Bolster Material Composition**

Material	Input [kg]	Finished Part [kg]	Finished Part [%]
Bolster	4.536	3.978	97%
<i>Polypropylene</i>	2.449	2.148	54%
<i>Glass fiber</i>	1.633	1.432	36%
<i>Small glass woven patch</i>	0.454	0.398	10%
Steel fasteners	0.136	0.1360	3%
<b>Total</b>	<b>4.672</b>	<b>4.114</b>	<b>100%</b>

#### 4.1.4 Production

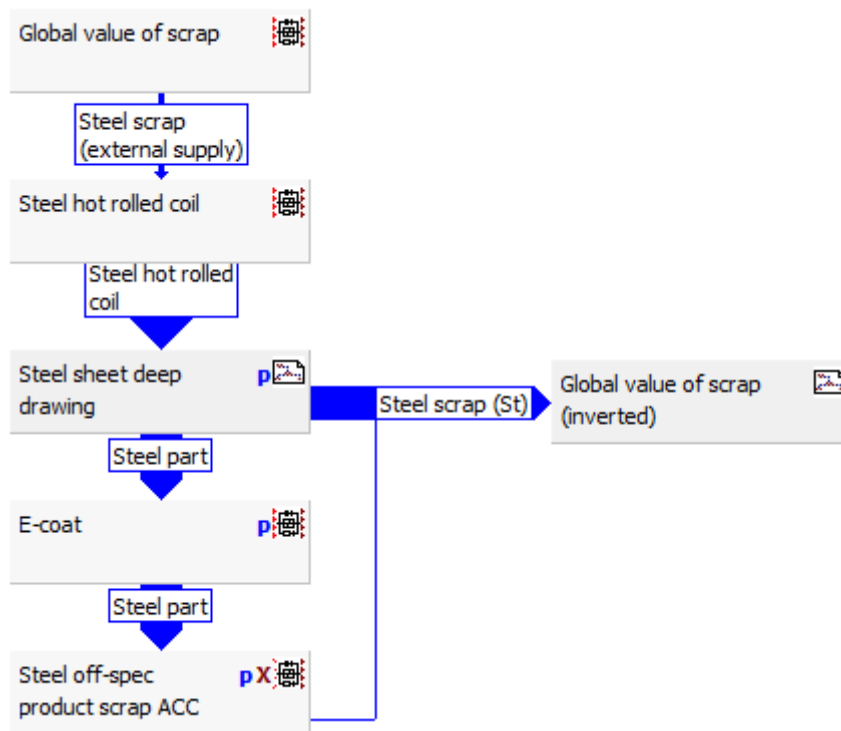
Production of steel components (excluding fasteners) in all models consists of cradle-to-gate production of the hot rolled steel coil, part production, and e-coat, as shown in Figure 2.

The 2010 Worldsteel Association (worldsteel) LCI dataset for ungalvanized, hot rolled coil was used to represent the hot rolled steel sheet used in the manufacturing of the steel components in the auto parts. This dataset is the most recent global average production of hot rolled steel coil. worldsteel has taken an avoided burden approach and allocated a portion of the environmental impacts associated with primary steel production to steel scrap. In accordance with worldsteel's chosen methodology, the model applies the worldsteel "global value of scrap" as an upstream burden for the use of steel scrap, and likewise as an environmental credit for the production of available scrap for recycling (inverted "global value of scrap"). The value of scrap is calculated as the difference between producing a given amount of material by (hypothetical) 100 % primary production (blast oxygen furnace route) and the same amount of material through secondary production means.

An alternative to the avoided burden approach (aka end-of-life recycling) that is also ISO-compliant and frequently used in LCA studies is the cut-off approach (aka recycled content).<sup>9</sup> These two approaches represent two very different scenarios for end-of-life modeling since the avoided burden approach assumes that all the scrap generated (minus losses from collection and recycling) will actually displace primary steel production at some point in time, while the cut-off approach disregards any assumptions about possible future benefits and simply incentivizes the use of recycled content today. Section 6.3 presents the results using the cut-off approach, which has the scrap input undergo a recycling process ("DE: car shredder PE" dataset), but does not attribute any environmental burden from the primary production of the scrap. Likewise, there is no burden and no credit applied for recycling of steel scrap.

<sup>9</sup> For a discussion of these two approaches and their implications see Frischknecht, R. (2010): LCI modelling approaches applied on recycling of materials in view of environmental sustainability, risk perception and eco-efficiency, Int J Life Cycle Assess (2010) 15:666-671.

Steel part production is modeled using the PE dataset for steel sheet deep drawing, which is a multi-stage process, and requires inputs of power, thermal energy, and lubricants. The deep drawing dataset is adjusted to account for the reported scrap amounts in Sections 4.1.1 to 4.1.2 above. E-coating (i.e., painting) is modeled using a PE dataset and requires inputs of dip coat, power, thermal energy, and deionized water, as well as wastewater treatment. The energy and other inputs required are calculated (scaled) according to the input material flows in Table 2 through Table 3. The datasets used for steel part production are shown in Table 5.



**Figure 2: Cradle-to-gate Production of Steel Part**

**Table 5: Datasets Used for Production of Steel Parts**

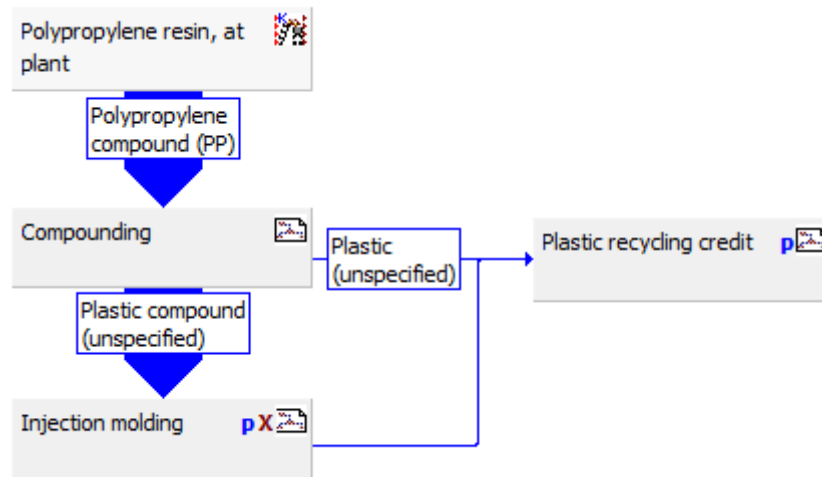
Category	Dataset	Nation/Region	Source	Reference Year
Materials	Car shredder (for cut-off approach)	DE	PE	2005
	Dip coat mix	DE	PE	2005
	Lubricants at refinery	US	PE	2003
	Steel hot rolled coil	GLO	worldsteel	2007
	Value of scrap (for avoided burden approach)	GLO	worldsteel	2007
	Water deionized	US	PE	2005
Part production	Application dip coat (EC; automobile)	DE	PE	2005
	Steel sheet deep drawing	DE	PE	2005
Energy	Power grid mix	US	PE	2002
	Thermal energy from natural gas	US	PE	2002
Disposal	Municipal sewage plant	US	PE	2006

Production of plastic parts consists of production of the materials, compounding, and part production, as shown for example in Figure 3. The datasets used for plastic part production are shown in Table 6.

As noted in Section 3.5.2, ACC plastics data as available in the NREL USLCI database were used when available to represent the plastics materials used in manufacturing. The ACC dataset used in this study was for polypropylene resin. This dataset is compared to the PE dataset for US polypropylene granulate in Section 6.4.

Part production is modeled using the PE dataset for injection molding, and adjusted to account for the reported scrap amounts in Sections 4.1.1 to 4.1.3 above. Injection molding requires power input, and landfilling of waste material. Compounding requires power and water inputs, and wastewater treatment. The energy and other inputs required are calculated (scaled) according to the input material flows in Table 2 through Table 4.

For the plastic components, the scrap is sent to a recycler and modeled using the avoided burden approach, by applying a recycling process (“US: Plastic granulate secondary” dataset) and a credit for plastic scrap (inverse of the appropriate plastic dataset). No scrap input is required as the parts are comprised of primary plastic material. Additionally, Section 6.3 presents the results using the cut-off approach, which does not apply credits for scrap.



**Figure 3: Cradle-to-gate Production of Plastic Part**

**Table 6: Datasets Used for Production of Plastic Parts**

Category	Dataset	Nation/ Region	Source	Reference Year
Materials	Glass fibres	US	PE	2005
	Nylon 6 granulate (PA 6)	US	PE	2005
	Plastic granulate secondary (nonspecific) (for avoided burden approach)	US	PE	2005
	Polypropylene (PP) virgin resin	RNA	USLCI	2011
Part production	Compounding (plastics)	GLO	PE	2005
	Plastic injection moulding part	DE	PE	2005
Energy	Power grid mix	US	PE	2002
Disposal	Landfill for inert matter (Construction waste)	DE	PE	2005
	Municipal sewage plant	US	PE	2006

Additionally, datasets used for the fasteners are shown in Table 7.

**Table 7: Datasets Used for Fasteners**

Material	Dataset	Nation/ Region	Source	Reference Year
Aluminum fastener	Aluminum sheet mix	RER	PE	2002
Brass fastener	Brass component	DE	PE	2005
Steel fastener	Fixing material screws galvanized	DE	PE	2005

Although no transportation data were collected, transportation of raw materials and transportation of final product were modeled assuming a distance of 300 miles by truck using the GaBi 4 database.

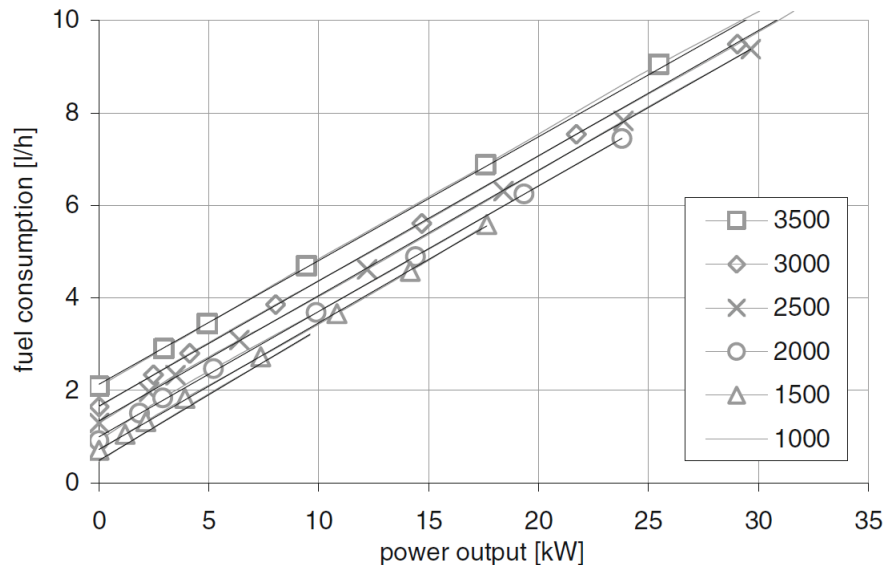
## 4.2 CALCULATION OF USE PHASE FUEL SAVINGS

For the use phase, fuel savings due to lightweight design over the assumed vehicle lifetime mileage of 150,000 miles is calculated based on the EPA city and highway standard driving cycles and the differential efficiency of gasoline engines, using the methodology described in *Koffler & Rohde-Brandenburger (2010)*.<sup>10</sup> The method is based on the *amount of work* necessary to move a certain weight through a certain driving cycle, and the *differential efficiency* of the internal combustion engine. The differential efficiency expresses the increase in an engine's fuel consumption for providing an additional power output while it is running. It can be visualized using the so-called Willans lines, which plot the fuel consumption in [liters/hour] over the respective power output [kW] for different rpm levels.

As can be seen in Figure 4, the differential efficiencies (i.e., the slopes of the Willans lines) are virtually the same for low power outputs and low rpms (< 4000 rpm), which are typical for most fuel economy driving cycles. It has been shown that the differential efficiency of engines with the same

<sup>10</sup> Koffler C, Rohde-Brandenburger K (2010): On the calculation of fuel savings through lightweight design in automotive life cycle assessments, *Int J Life Cycle Assess* (2010) 15:128-135

working process is, in contrast to their overall efficiency, very similar.<sup>11</sup> For naturally aspirated gasoline engines, the ascertained average is 0.264 (l/h)/kW or 0.073 l/MJ. By combining these values with the respective *mass-induced energy demand* for moving a certain weight through a certain driving cycle, the *mass-induced fuel consumption* can be calculated.



**Figure 4: Willans lines of a 1.4 l turbo-charged gasoline engine (90 kW) for low output and low rpm<sup>12</sup>**

In order to do so, first the mass induced energy demand needs to be calculated using the following formula:

$$W_{\text{sum}} = m * ((1 - d) * g * f_R * C_{WR} + C_{Wa})$$

with

$W_{\text{sum}}$ : energy demand [MJ]

$m$ : mass [kg]

$d$ : share of deceleration phases in driving cycle [%]

$g$ : gravitational constant [ $\text{m/s}^2$ ]

<sup>11</sup> Rohde-Brandenburger K (1996): Verfahren zur einfachen und sicheren Abschätzung von Kraftstoffverbrauchs-potentialen, Einfluss von Gesamtfahrzeugparametern auf Fahrzeugverhalten/Fahrleistung und Kraftstoffverbrauch. Haus der Technik, Essen

<sup>12</sup> Koffler C, Rohde-Brandenburger K (2010): On the calculation of fuel savings through lightweight design in automotive life cycle assessments, Int J Life Cycle Assess (2010) 15:128-135



$f_R$ : rolling resistance coefficient (dimensionless)

$C_{WR}$ : constant for rolling resistance [m]; specific to driving cycle

$C_{Wa}$ : constant for acceleration resistance [ $m^2/s^2$ ]; specific to driving cycle

The *mass induced energy demand* for the US combined fuel economy driving cycle<sup>13</sup> for 100 km and 100 kg therefore is:

$$\begin{aligned} W_{\text{sum}(100 \text{ kg}, 100 \text{ km})} &= (100 \text{ km} / 17.2 \text{ km}) * m * ((1 - d) * g * f_R * C_{WR} + C_{Wa}) \\ &= (100 \text{ km} / 17.2 \text{ km}) * 100 \text{ kg} * (0.83 * 9.81 \text{ m/s}^2 * 0.01 * 17,198 \text{ m} + 2,221 \text{ m}^2/\text{s}^2) \\ &= \mathbf{2.1 \text{ MJ}} \end{aligned}$$

with 17.2 kilometers being the combined distance of the EPA city and highway driving cycle (55% \* 11.04 miles + 45% \* 10.26 miles) and 17% being the combined deceleration phases of both (55% \* 25% + 45% \* 8%).<sup>14</sup>

Assuming a conservative 5% losses in the automatic gearbox,<sup>15</sup> the *mass-induced fuel consumption* for naturally aspirated gasoline engines for the US EPA combined driving cycle for 100 kg is:

$$\begin{aligned} V_{100 \text{ kg}} &= 2.1 \text{ MJ} * 1.05 * 0.073 \text{ l/MJ} \\ &= 0.161 \text{ l}/(100 \text{ km} * 100 \text{ kg}) \\ &= \mathbf{0.031 \text{ gal}/(100 \text{ mi} * 100 \text{ lb})} \end{aligned}$$

The above calculations assume that no constructive changes are made to the vehicle itself. They correspond to the amount of mass-induced fuel consumption in a given driving cycle, and vice versa to the reduction in fuel consumption when that weight is removed from the vehicle, e.g. empty trunk vs. full trunk. The latter *fuel reduction value* (i.e., the fuel saving in comparison to a given reference) is significantly increased when one considers unchanged vehicle performance as an objective to preserve functional equivalence on the system level before and after the lightweighting measure.

In theory, each mass reduction improves the vehicle's acceleration and dynamic performance. An adaptation of the drive train (i.e., the reduction of engine capacity or the elongation of the gear ratio) may therefore further increase the fuel economy while preserving the vehicle dynamics. A multitude of simulations of drive train adaptations rendered fuel reduction values that are a factor 1.9 to 3.0 higher than the values without additional drive train adaptations (avg: 2.37).<sup>16</sup>

<sup>13</sup> 55% city /45% highway

<sup>14</sup> Assumption: decelerations are strong enough to allow engine to enter throttle cutoff mode.

<sup>15</sup> Schlegel et al (2009): Detailed Loss Modelling of Vehicle Gearboxes, Proceedings 7th Modelica Conference, Como, Italy, Sep. 20-22, 2009. Available at <http://www.ep.liu.se/ecp/043/048/ecp09430059.pdf>

<sup>16</sup> Koffler C, Rohde-Brandenburger K (2010): On the calculation of fuel savings through lightweight design in automotive life cycle assessments, Int J Life Cycle Assess (2010) 15:128-135

Assuming the ratio between no drive train adaptation and adapted drive train is about the same for the US combined driving cycle as for the New European Driving Cycle, the potential decrease in fuel consumption with adaptation for naturally aspirated gasoline engines amounts to:

$$V_{100 \text{ kg}}^* = 0.031 \cdot 2.37 = \mathbf{0.07 \text{ gal}/(100 \text{ mi} \cdot 100 \text{ lb})}$$

Carbon dioxide emissions from fuel combustion are then calculated using the average emission factor provided by the US EPA of 19.4 pounds per gallon of gasoline.<sup>17</sup> Sulfur dioxide emissions are calculated based on the fuels' sulfur content (30 ppm).<sup>18</sup>

Due to the fact that there is not sufficient evidence that

- a) the sum of all lightweight design measures in the car (which are unknown) would actually allow for a drivetrain adaptation in real life, and
- b) that the involved car manufacturers actually prefer fuel economy over performance within the design process,

the adapted fuel reduction value is only considered in a what-if scenario in this study. Chapter 5 therefore presents the results with no adaptation to the drive train, while Section 6.1 presents the results for an adapted drive train. In addition, the following key assumptions are tested in a subsequent sensitivity analysis in Section 6.2: share of deceleration phases (17%), rolling resistance (0.01), automatic gearbox loss (5%), and the ratio of savings with an adapted drive train to no adaptation (2.37).

### 4.3 END-OF-LIFE TREATMENT

It is assumed that 98% of the steel material is recovered for recycling at end-of-life. The recycled steel is awarded a recycling credit defined by the worldsteel "global value of scrap" dataset. In addition, Section 6.3 provides the results using the cut-off approach, which does not apply a steel recycling credit or any primary upstream burden for scrap inputs in manufacturing.

It is assumed that all plastic material is landfilled, as represented by the PE dataset "RER: Landfill for inert matter (Construction waste)."

<sup>17</sup> U.S. Environmental Protection Agency (2005): Average Carbon Dioxide Emissions Resulting from Gasoline and Diesel Fuel, available at: <http://www.epa.gov/oms/climate/420f05001.htm#calculating>

<sup>18</sup> U.S. Environmental Protection Agency (2009): Gasoline Sulfur Standards, available at: <http://www.epa.gov/oms/standards/fuels/gas-sulfur.htm>

U.S. Environmental Protection Agency (2009): Highway, Nonroad, Locomotive, and Marine Diesel Fuel Sulfur Standards, available at: <http://www.epa.gov/oms/standards/fuels/diesel-sulfur.htm>

## 5 RESULTS

This chapter presents the potential environmental impacts for a vehicle lifetime of 150,000 miles. See Chapter 6 for scenario and sensitivity analyses.

The US EPA's TRACI impact categorization methodology was used for Eutrophication Potential, Acidification Potential, and Smog Potential. A recent update of the IPCC factors for climate change is not reflected in the TRACI characterization factors, so CML factors (which were updated with IPCC data in November 2009) were used to evaluate Global Warming Potential. The recently released USEtox methodology was used to calculate human toxicity and ecotoxicity potential. Primary energy demand from non-renewable resources was also included. Each of these impact categories is further described in Appendix A: Life Cycle Impact Assessment Categories.

The potential environmental impacts for each product are broken down into 3 life cycle stages:

- Manufacturing:
  - Cradle-to-gate materials and part production including transport
  - Credit for scrap generation
- Use:
  - Cradle-to-gate fuel production (pre-combustion)
  - Fuel combustion emissions
- End-of-life:
  - Landfill
  - Credit for scrap generation

The difference between the baseline product (2008 bolster) and the alternative products (2005 and 2010 bolsters) is calculated as the alternative product results minus the baseline product results. The use phase emissions are only calculated as a difference from the baseline. Thus the use phase impact is zero for the baseline product and carries a negative sign for the comparison products, which weigh less than the baseline product, resulting in less fuel consumption and combustion emissions.

The values for scrap generation carry a negative sign because the model provides a “credit” for the avoided production of primary steel and plastic (avoided burden approach). These are only potential credits, as there is no certainty that the material will be recycled at the end of its life. Additionally, Section 6.3 provides the results using the cut-off approach.

Appendix C: Detailed Manufacturing Results shows the manufacturing results not including transport by component (credits included) and by material or process (credits shown separately).

Normalization is an optional step within LCA used to help interpret the relative significance of the multiple environmental indicators. The latest TRACI normalization factors<sup>19</sup> are applied in order to convert the various units of each individual environmental indicator into a common, dimensionless

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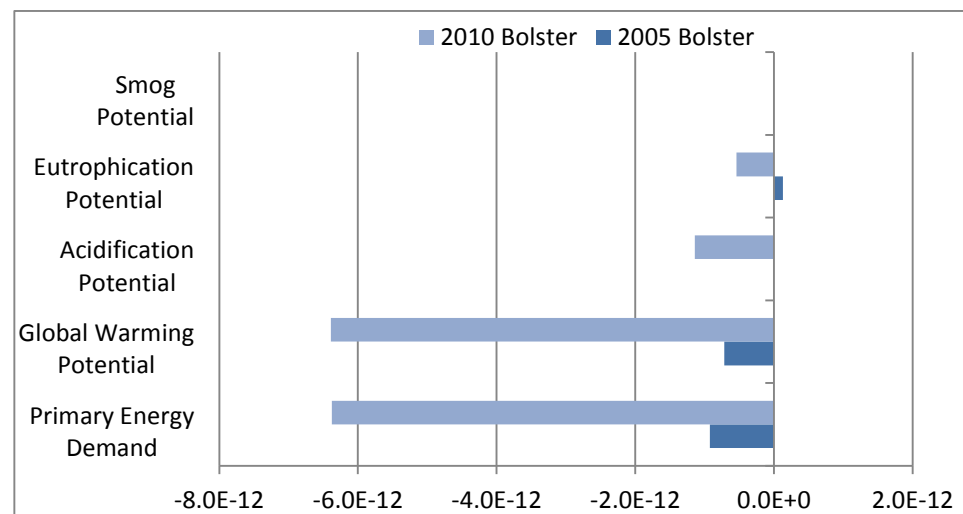
<sup>19</sup> Bare et al: Development of the Method and U.S. Normalization Database for Life Cycle Impact Assessment and Sustainability Metrics, Environmental Science & Technology (2006) 40:5108-5115

scale. The normalization factors are based upon the 1999 annual total US emissions contributing to each of the TRACI environmental indicators. The 1999 total non-renewable energy consumption available from the Energy Information Administration<sup>20</sup> is applied to normalize non-renewable primary energy demand. Table 8 provides the normalization factors.

**Table 8: TRACI Normalization Factors**

Impact Category	Normalization Factor
Primary Energy Demand (net calorific value) [MJ]	9.50E+13
Global Warming Potential (100 years) [kg CO <sub>2</sub> -Equiv.]	6.85E+12
Acidification Potential [mol H <sup>+</sup> Equiv.]	2.08E+12
Eutrophication Potential [kg N-Equiv.]	5.02E+09
Smog Potential [kg NO <sub>x</sub> -Equiv.]	3.38E+10

Figure 5 shows that when comparing to the baseline 2008 bolster for the selected environmental indicators, smog potential is marginal and eutrophication potential is rather low compared to primary energy demand, global warming potential, and acidification potential. Therefore the following sections focus on primary energy demand, global warming potential, and acidification potential and the results for smog and eutrophication potential are provided in Appendix D: Results for Eutrophication and Smog Potential.



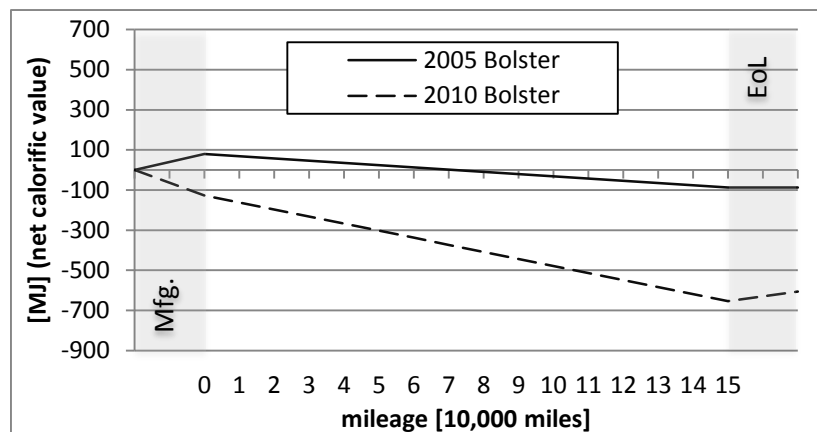
**Figure 5: Bolster Normalized TRACI Environmental Indicators – Alternative Minus Baseline**

Table 9 through Table 11 show the life cycle performance of the 2008 front end bolster (baseline product) and the 2005 and 2010 bolsters (alternative products) and the difference from baseline (alternative product results minus baseline product results) for non-renewable primary energy demand, global warming potential, and acidification potential. Figure 6 through Figure 8 show the difference from the baseline throughout the life cycle of the vehicle and if there is a “break-even” mileage where the baseline and comparison product are equal in potential impact i.e., the impact equals zero.

<sup>20</sup> U.S. Energy Information Administration (2011): Monthly Energy Review. Available at: [http://www.eia.gov/emeu/mer/pdf/pages/sec1\\_3.pdf](http://www.eia.gov/emeu/mer/pdf/pages/sec1_3.pdf)

**Table 9: Bolster Primary Energy Demand**

Primary Energy Demand (net calorific value) [MJ]	Absolute Results			Alternative Minus Baseline	
	2008 Bolster	2005 Bolster	2010 Bolster	2005 Bolster	2010 Bolster
Manufacturing	558.80	639.03	432.22	80.24	-126.57
Materials/Part Production	632.75	694.28	459.55	61.53	-173.20
Scrap Credit	-73.95	-55.25	-27.33	18.71	46.62
Use	n/a	n/a	n/a	-166.90	-528.07
Fuel Production (Pre-combustion) <sup>21</sup>	n/a	n/a	n/a	-166.90	-528.07
Fuel Combustion Emissions	n/a	n/a	n/a	0	0
EoL	-50.21	-51.17	-1.08	-0.97	49.13
Landfill	0.64	0.46	0.64	-0.19	0
Scrap Credit	-50.85	-51.63	-1.72	-0.78	49.13
<b>Total</b>	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>-87.63</b>	<b>-605.52</b>



**Figure 6: Bolster Primary Energy Demand – Alternative Minus Baseline**

**Table 10: Bolster Global Warming Potential**

Global Warming Potential (GWP 100 years) [kg CO <sub>2</sub> -Equiv.]	Absolute Results			Alternative Minus Baseline	
	2008 Bolster	2005 Bolster	2010 Bolster	2005 Bolster	2010 Bolster
Manufacturing	34.83	42.28	24.76	7.45	-10.07
Materials/Part Production	41.94	47.44	25.94	5.50	-16.00
Scrap Credit	-7.11	-5.17	-1.18	1.95	5.94
Use	n/a	n/a	n/a	-12.34	-39.03
Fuel Production (Pre-combustion)	n/a	n/a	n/a	-2.38	-7.53
Fuel Combustion Emissions	n/a	n/a	n/a	-9.95	-31.49
EoL	-5.32	-5.43	-0.10	-0.11	5.22
Landfill	0.08	0.06	0.08	-0.02	0.00
Scrap Credit	-5.40	-5.49	-0.18	-0.08	5.22
<b>Total</b>	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>-4.99</b>	<b>-43.87</b>

<sup>21</sup> The “alternative minus baseline” energy content of the gasoline used by the vehicle is 83% of the primary energy demand. The remainder of the primary energy demand is from the processing required to produce the fuel.

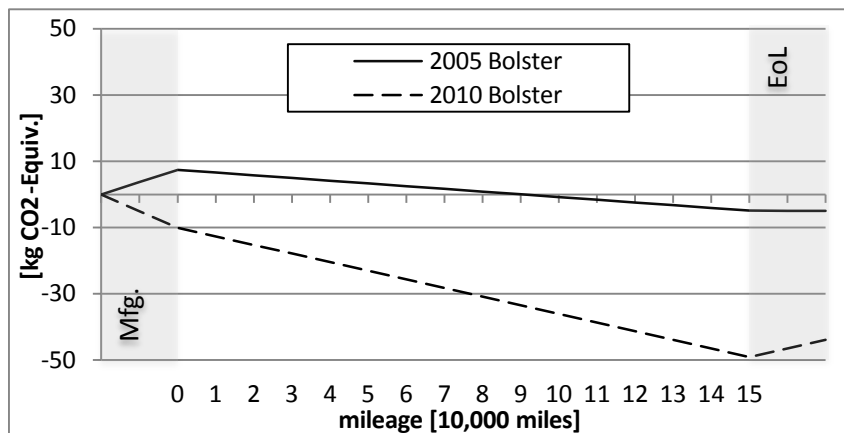


Figure 7: Bolster Global Warming Potential – Alternative Minus Baseline

Table 11: Bolster Acidification Potential

Acidification Air [mol H+ Equiv.]	Absolute Results			Alternative Minus Baseline	
	2008 Bolster	2005 Bolster	2010 Bolster	2005 Bolster	2010 Bolster
Manufacturing	7.31	6.10	6.10	-1.21	-1.21
Materials/Part Production	8.07	6.61	6.37	-1.46	-1.70
Scrap Credit	-0.76	-0.51	-0.27	0.25	0.49
Use	n/a	n/a	n/a	-0.53	-1.68
Fuel Production (Pre-combustion)	n/a	n/a	n/a	-0.52	-1.65
Fuel Combustion Emissions	n/a	n/a	n/a	0	0
EoL	-0.52	-0.53	0.00	-0.01	0.52
Landfill	0.02	0.01	0.02	-0.01	0
Scrap Credit	-0.53	-0.54	-0.02	-0.01	0.52
<b>Total</b>	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>-1.76</b>	<b>-2.37</b>

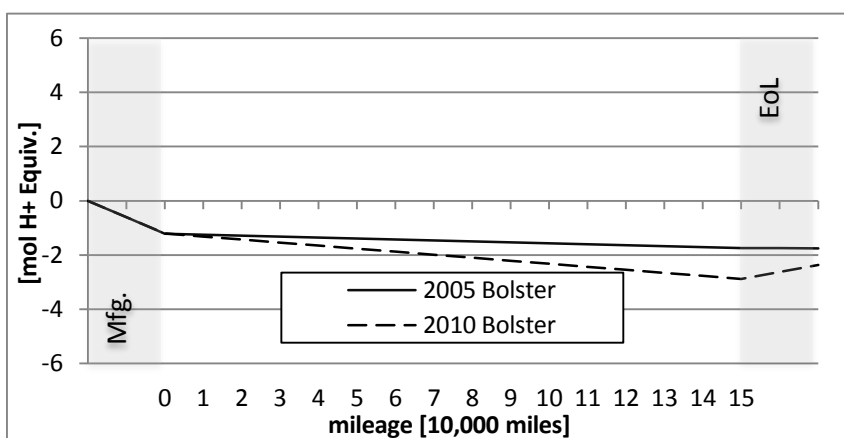


Figure 8: Bolster Acidification Potential – Alternative Minus Baseline

Compared to the 2008 front end bolster (baseline), cradle-to-gate production of the 2005 bolster has a higher environmental burden for primary energy demand and global warming potential even though it weighs 14% less than the 2008 bolster (6.496 kg vs. 7.597 kg). This lighter weight causes a

decrease in impact during the use stage over the vehicle lifetime, eventually reaching a break-even distance between 70,000 and 80,000 miles for primary energy demand and 90,000 and 100,000 miles for global warming potential. The 2005 bolster remains lower over the vehicle lifetime for acidification potential. The end-of-life stage is negligible.

The use phase is separated into the cradle-to-gate production of gasoline (pre-combustion) and the gasoline combustion air emissions. For both the 2005 and 2010 comparison to the baseline, the difference from baseline is mostly from the production of gasoline for acidification potential and from combustion emissions for global warming potential. The emissions calculated for combustion were carbon dioxide and sulfur dioxide, which affect global warming and acidification potential, respectively.

The cradle-to-gate production of the 2010 bolster has a lower impact than the 2008 bolster for all impact categories. As it weighs 46% less than the 2008 bolster (4.114 kg vs. 7.597 kg), it also has a significantly lower impact during the use stage over the vehicle lifetime. The use phase is the dominant life cycle stage in the comparison.

Compared to the baseline, the 2010 bolster end-of-life potential impact is higher for all impact categories. It has less material going to recycling per product (0.1 kg vs. 3.6 kg). The end-of-life stage contributes the least to the difference from the baseline.

For the 2008 bolster and for the 2005 bolster the majority of the ecotoxicity potential comes from sulfuric acid emissions to water from the hot rolled steel dataset. For the 2010 bolster the majority of the ecotoxicity potential comes from nitrogen oxides to air from the DLFT/glass mat part.

For the 2008 and 2010 bolsters the majority of the human toxicity potential comes from formaldehyde emissions to air from the plastic part production power consumption, i.e., the incomplete combustion of fuels during the production of electricity upstream. For the 2005 bolster the majority comes from formaldehyde emissions to air from the precursor to nylon 6, caprolactam from sulfur hexane.

## 6 SCENARIO AND SENSITIVITY ANALYSIS

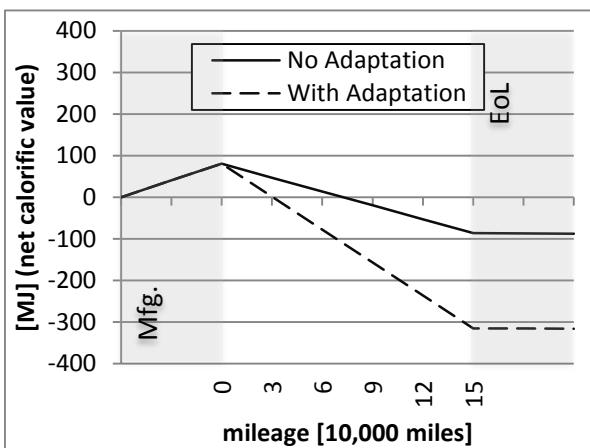
### 6.1 POWER TRAIN ADAPTATION SCENARIO

This section presents the life cycle performance of the 2005 and 2010 bolsters compared to the 2008 baseline (alternative product results minus baseline product results) if adjustments are made to the engine or gearbox due to the reduction in vehicle weight. It assumes that reduction of fuel consumption with drive train adaptation is 2.37 times higher than without adaptation, causing a greater difference in impact from the baseline product (see Section 4.2).

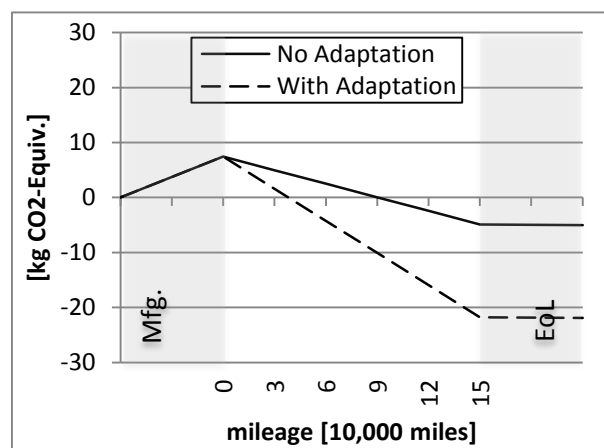
Table 12 reports the total life cycle potential impact difference from baseline (2008 bolster) with adaptation to the power train. Figure 9 through Figure 14 compare the no adaptation and with adaptation difference from baseline results. As expected, the lightweight products perform better when adaptation is taken into account.

**Table 12: Bolster with Adaptation – Alternative Minus Baseline**

Bolster with Adaptation - Alternative Minus Baseline	2005 Bolster	2010 Bolster
Primary Energy Demand (net calorific value) [MJ]	-316.29	-1328.96
Global Warming Potential (100 years) [kg CO <sub>2</sub> -Equiv.]	-21.89	-97.34
Acidification Potential [mol H <sup>+</sup> Equiv.]	-2.48	-4.67

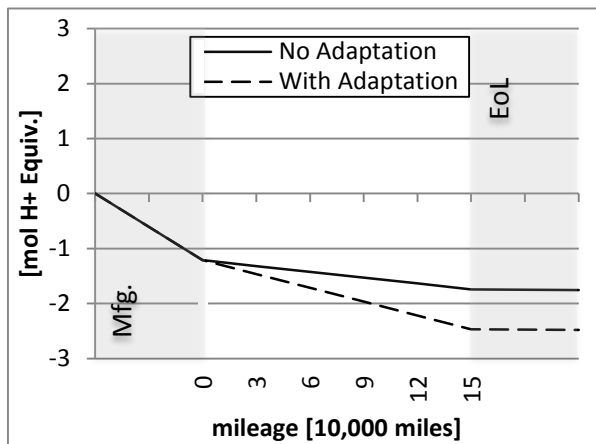


**Figure 9: 2005 Bolster Adaptation Primary Energy Demand – Alternative Minus Baseline**

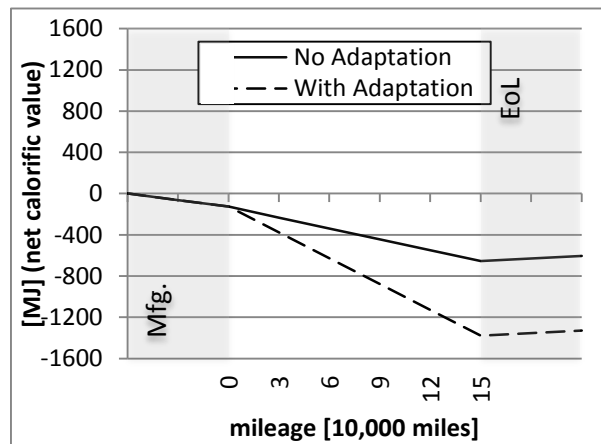


**Figure 10: 2005 Bolster Adaptation Global Warming Potential – Alternative Minus Baseline**

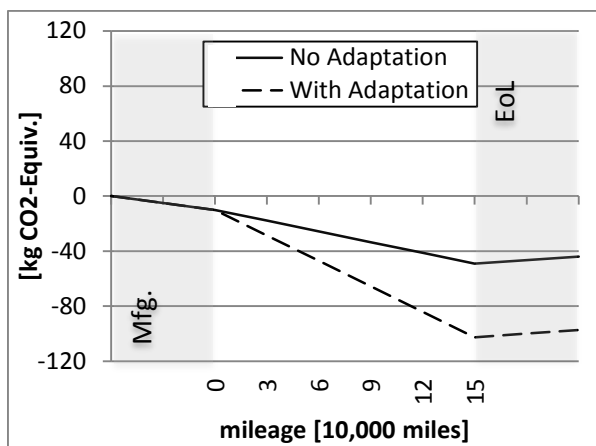




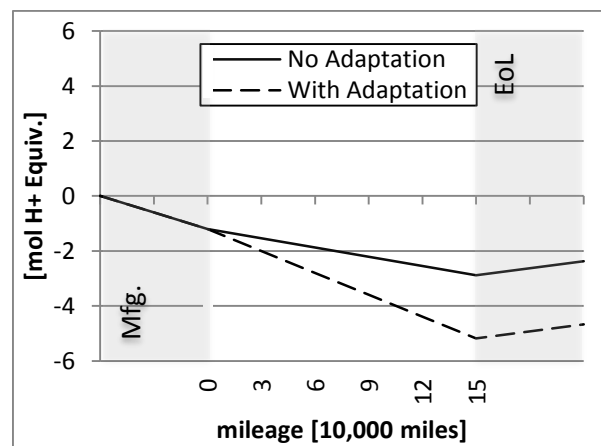
**Figure 11: 2005 Bolster Adaptation Acidification Potential – Alternative Minus Baseline**



**Figure 12: 2010 Bolster Adaptation Primary Energy Demand – Alternative Minus Baseline**



**Figure 13: 2010 Bolster Adaptation Global Warming Potential – Alternative Minus Baseline**



**Figure 14: 2010 Bolster Adaptation Acidification Potential – Alternative Minus Baseline**

## 6.2 CALCULATION OF USE PHASE FUEL SAVINGS UNCERTAINTY

The calculation of the potential use phase reductions in fuel consumption is based on a variety of uncertain input parameters, as described in Section 4.2. Monte Carlo analysis is a technique that propagates known parameter uncertainties through a calculation to give an uncertainty distribution of the output variables. It is based on random sampling from defined distributions around each uncertain input parameter. These distributions can either be determined based on empirical data or estimated based on expert judgment. Consequently, Monte Carlo analysis is an ideal method for quantifying the combined effect of parameter uncertainty in LCA studies, and is widely recognized and used in the LCA community.<sup>22,23,24</sup>

<sup>22</sup> Huijbregts MAJ, Gilijamse W, Ragas AMJ, Reijnders L (2003): Evaluating Uncertainty in Environmental Life-Cycle Assessment; *Environmental Science and Technology* 37, pp 2600 – 2608.

<sup>23</sup> Peters GP (2007): Efficient Algorithms for Life Cycle Assessment, Input-Output Analysis, and Monte-Carlo Analysis; *International Journal of Life Cycle Assessment* 12 (6), pp 373 - 380

<sup>24</sup> Lloyd SM, Ries R (2007): Characterizing, Propagating, and Analyzing Uncertainty in Life-Cycle Assessment; *Journal of Industrial Ecology*, Vol. 11, No. 1, pp 161 - 179

The least sophisticated form of a Monte Carlo simulation is the definition of upper and lower bounds via literature research or expert judgment for each parameter and the assumption of a uniform distribution between these boundaries. This allows for the approximation of the combined effect of uncertainties around parameters that have the potential to either add up or cancel each other out (i.e., they display different forms of proportional or inverse proportional relationships with the end result).

This type of Monte Carlo simulation can therefore be seen as a kind of parameter variation, but with random variation of multiple parameters instead of a step-wise variation of a single parameter. It renders more information than simple best case / worst case calculations as it provides an indication of where between these two extremes the results are to be expected.<sup>25</sup>

Table 13 shows the key parameters of the fuel savings calculation that were varied in the Monte Carlo simulations to assess the combined effect of their respective uncertainties on the final results:

- The assumption that the deceleration phases in the EPA combined cycle are strong enough to allow the engine to enter throttle cutoff mode (zero fuel consumption), which poses a conservative assumption in favor of the metal parts, was varied to be valid for values between 0% of the driving cycle and the base case value.
- The rolling resistance coefficient of 0.01 from Koffler & Rohde-Brandenburger (2010) was varied from 0.007 to 0.014 according to the typical range of available tires.<sup>26</sup>
- The 5% base case for automatic transmission losses is also a conservative assumption in favor of the metal parts since it represents the lower end of the range of gearbox losses for automatic transmissions.<sup>27</sup> The upper boundary of 10% was therefore also included in the Monte Carlo simulation.
- The uncertainty intervals around the fuel savings ratios (i.e., the ratio of FRV with adaptation to FRV without adaptation) were calculated using the maximum deviation between the average FRV values reported in Koffler & Rohde-Brandenburger (2010) and the likewise reported minimum and maximum FRVs from simulations. The largest ratio found was 29%; the interval used in the Monte Carlo simulation was therefore set to +/- 30% around the base scenario setting.

**Table 13: Intervals in Use Phase Monte Carlo Simulation (10,000 runs, uniform distribution)**

Parameter	Lower Limit	Base Scenario	Upper Limit
Deceleration in city driving cycle (no fuel consumption) [%]	0 <sup>b</sup>	25	25 <sup>w</sup>
Deceleration in highway driving cycle (no fuel consumption) [%]	0 <sup>b</sup>	8	8 <sup>w</sup>
$f_R$ , rolling resistance coefficient	0.007 <sup>w</sup>	0.01	0.014 <sup>b</sup>
Automatic gearbox losses [%]	5 <sup>w</sup>	5	10 <sup>b</sup>
Ratio of fuel savings with adaptation to no adaptation (gasoline)	1.66 <sup>w</sup>	2.37	3.08 <sup>b</sup>

<sup>w</sup>: worst-case specification; <sup>b</sup>: best-case specification

<sup>25</sup> In layman's terms, it means shooting at a large enough target with a shotgun, and then establishing the marksman's accuracy based on the average distance to the bull's eye across all bullet holes along with its standard deviation, instead of just calculating the minimum and maximum distance to be expected.

<sup>26</sup> Transportation Research Board (2006): Tires and Passenger Vehicle Fuel Economy; Special Report 286, Washington DC. Available at <http://onlinepubs.trb.org/onlinepubs/sr/sr286.pdf>

<sup>27</sup> Schlegel C, Hoesl A, Diel S (2009): Detailed Loss Modeling of Vehicle Gearboxes, Proceedings of the 7th Modelica Conference, Como, Italy, Sep. 20-22, 2009. Available at <http://www.ep.liu.se/ecp/043/048/ecp09430059.pdf>

Since there are no data indicating that any value from the above intervals is more likely than any other value from the same interval, a uniform distribution is assumed for each of them. The assessment of the combined uncertainties is nevertheless indicated as (a) some of the parameters have an inverse proportional relationship with the results, meaning that an the effect of an increase of one parameter may be cancelled out by an increase of another parameter, and (b) not all base scenario parameter settings are situated in the center of the ascertained uncertainty intervals.

By propagating these uncertainties simultaneously a multitude of times using random sampling (here: 10,000 runs), the Monte Carlo simulation provides a better estimate of the uncertainty of the fuel reduction potential.<sup>28</sup> The according standard deviations will also give a better indication of the more likely range of results than simple best case / worst case calculations.

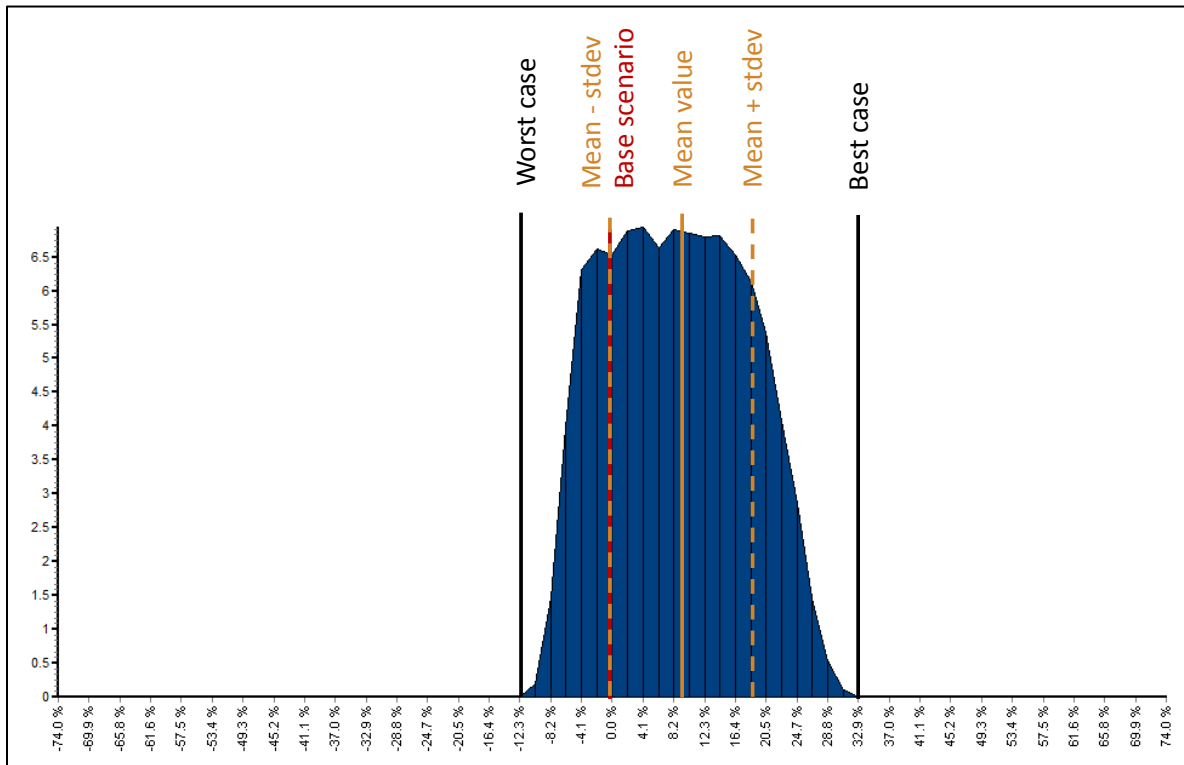
As displayed in Figure 15 and Figure 16, the resulting mean fuel reduction potential was 9% higher than for the base scenario (red line) across all 10,000 runs, both without and with drive train adaptation. Without drive train adaptation, the standard deviation around the ascertained mean was +/- 9%; with inclusion of drive train adaptation, it increased to +/- 19%. Thus the base scenario results shown in Chapter 5 appear to be conservative approximations to the mass-induced fuel savings.

Figure 15 and Figure 16 also display the best and worst case results according to the parameter specifications indicated in Table 13. Accordingly, the worst possible fuel reduction would be 12 % lower than the base case (38 % lower if drive train adaptations are considered), while the best possible fuel reduction would be 33 % higher than the base case (73 % higher if drive train adaptations are considered).

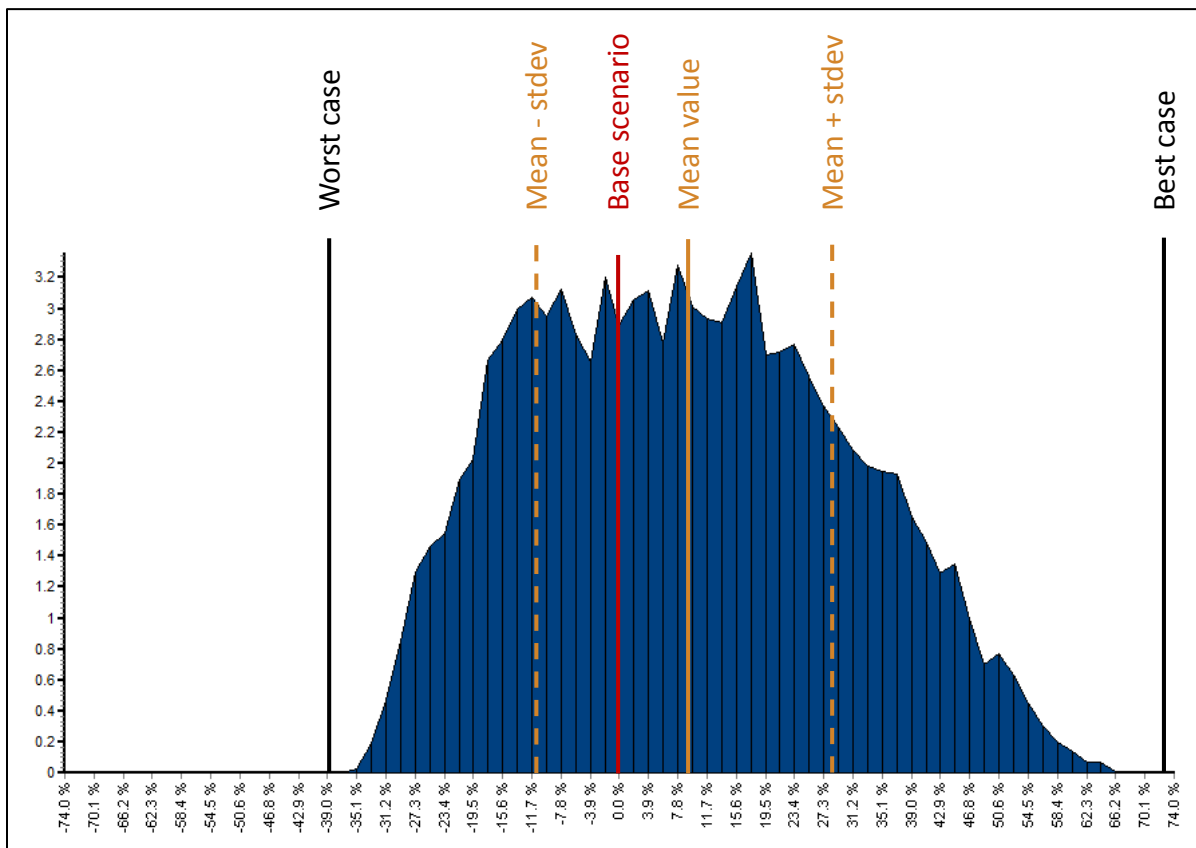
This comparison again illustrates the benefit of the Monte Carlo simulation over a simple worst-case / best-case scenario: instead of quantifying only the upper and lower limit of the uncertainty interval, its probability distribution, mean value and standard deviation are established based on random sampling. This provides the practitioner with a deeper understanding of the uncertainty.

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<sup>28</sup> Ciroth A, Fleischer G, Steinbach J (2004): Uncertainty Calculations in Life Cycle Assessments, International Journal of Life Cycle Assessment 9 (4), pp 216 - 226



**Figure 15: Fuel reduction potential - Monte Carlo simulation results without drive train adaptation**



**Figure 16: Fuel reduction potential - Monte Carlo simulation results with drive train adaptation**

Table 14 presents the difference from baseline results (alternative product minus baseline product) over the entire life cycle for the base scenario (Chapter 5) next to the results using the Monte Carlo mean value for the use phase. With an increase in fuel reduction potential the lightweight products perform better than they did in the base scenario.

**Table 14: Cradle-to-grave Base and Monte Carlo Scenarios – Alternative Minus Baseline**

Product	Impact Category	No adaptation		With adaptation	
		Base Scenario	Monte Carlo	Base Scenario	Monte Carlo
2005 Bolster	Primary Energy Demand (net calorific value) [MJ]	-87.63	-102.65	-316.29	-351.89
	Global Warming Potential (100 years) [kg CO <sub>2</sub> -Equiv.]	-4.99	-6.11	-21.89	-24.53
	Acidification Potential [mol H <sup>+</sup> Equiv.]	-1.76	-1.80	-2.48	-2.60
2010 Bolster	Primary Energy Demand (net calorific value) [MJ]	-605.52	-653.04	-1408.23	-1520.87
	Global Warming Potential (100 years) [kg CO <sub>2</sub> -Equiv.]	-43.87	-47.39	-104.68	-113.01
	Acidification Potential [mol H <sup>+</sup> Equiv.]	-2.37	-2.52	-3.44	-3.80

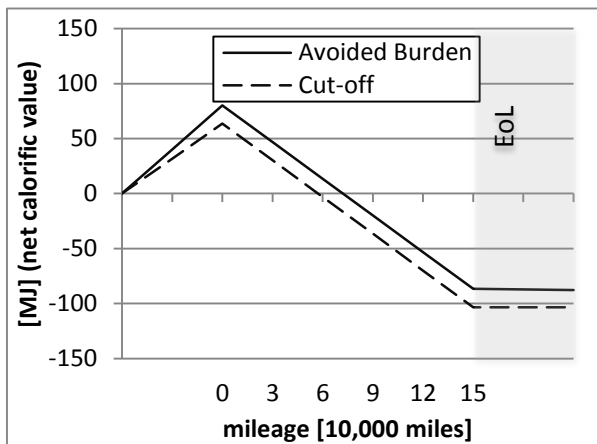
### 6.3 CUT-OFF APPROACH

Table 15 shows the life cycle performance of 2008 bolster (baseline product) and the 2005 and 2010 bolsters (alternative products) using the cut-off approach, and the difference from baseline (alternative product results minus baseline product results). The cut-off approach does not apply an environmental credit for the recycling of production scrap or material at end-of-life. Likewise, it does not apply an upstream burden for the use of steel scrap (worldsteel “global value of scrap” dataset described in Section 4.1.4); instead, only the recycling process is included.

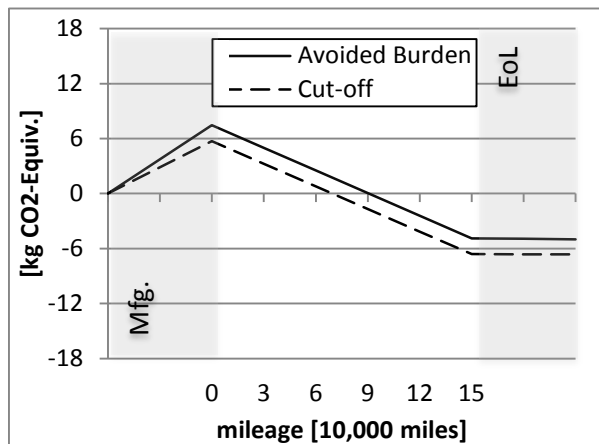
Figure 17 through Figure 22 show the difference from baseline results using avoided burden approach and cut-off approach throughout the vehicle life cycle. For all impact categories the lighter-than-baseline products performed better using cut-off approach when comparing to the baseline. Therefore the avoided burden results are conservative for comparing to the baseline product.

**Table 15: Bolster Results – Cut-off Approach**

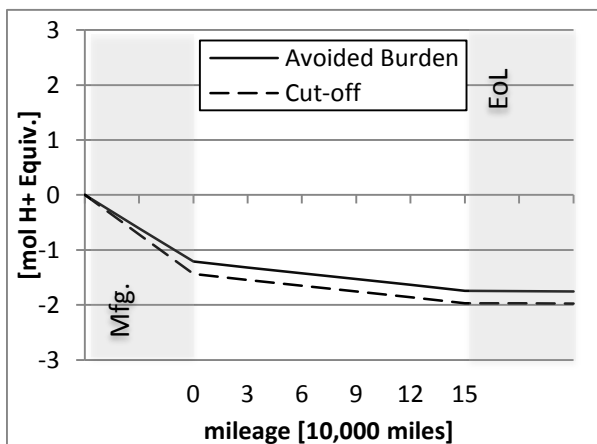
Impact Category	Life Cycle Stage	Absolute Results			Alternative Minus Baseline	
		2008 Bolster	2005 Bolster	2010 Bolster	2005 Bolster	2010 Bolster
Primary Energy Demand (net calorific value) [MJ]	Manufacturing	620.09	683.69	459.55	63.60	-160.54
	Use	n/a	n/a	n/a	-166.90	-528.07
	EoL	0.64	0.46	0.64	-0.19	0
	<b>Total</b>	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>-103.49</b>	<b>-688.61</b>
Global Warming Potential (100 years) [kg CO <sub>2</sub> -Equiv.]	Manufacturing	40.56	46.28	25.94	5.72	-14.62
	Use	n/a	n/a	n/a	-12.34	-39.03
	EoL	0.08	0.06	0.08	-0.02	0
	<b>Total</b>	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>-6.63</b>	<b>-53.65</b>
Acidification Potential [mol H <sup>+</sup> Equiv.]	Manufacturing	7.93	6.49	6.37	-1.44	-1.56
	Use	n/a	n/a	n/a	-0.53	-1.68
	EoL	0.02	0.01	0.02	-0.01	0
	<b>Total</b>	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>-1.97</b>	<b>-3.24</b>



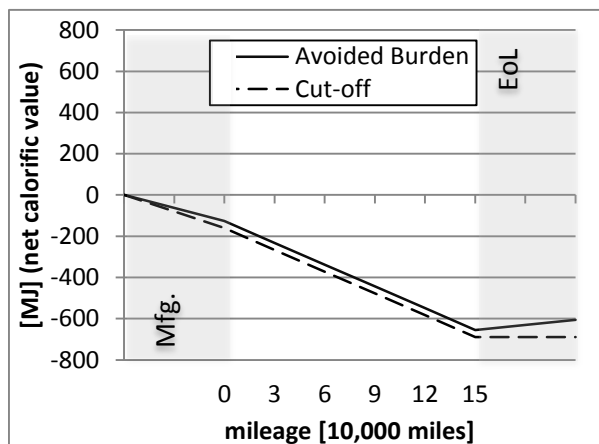
**Figure 17: 2005 Bolster Cut-off Primary Energy Demand – Alternative Minus Baseline**



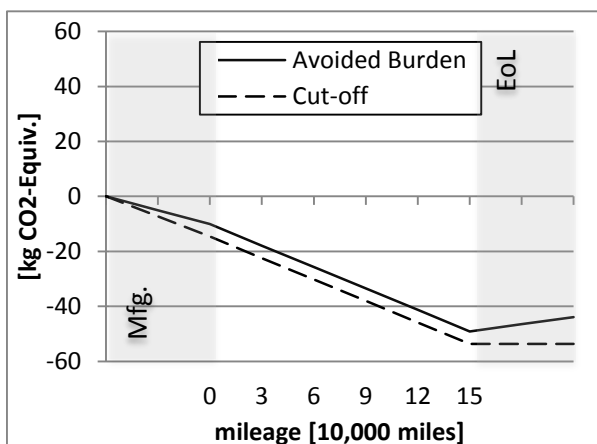
**Figure 18: 2005 Bolster Cut-off Global Warming Potential – Alternative Minus Baseline**



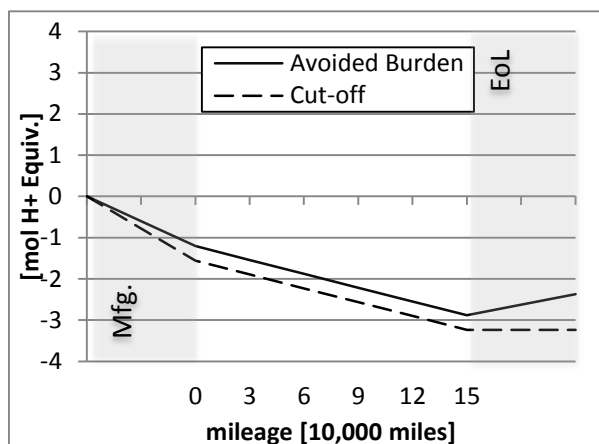
**Figure 19: 2005 Bolster Cut-off Acidification Potential – Alternative Minus Baseline**



**Figure 20: 2010 Bolster Cut-off Primary Energy Demand – Alternative Minus Baseline**



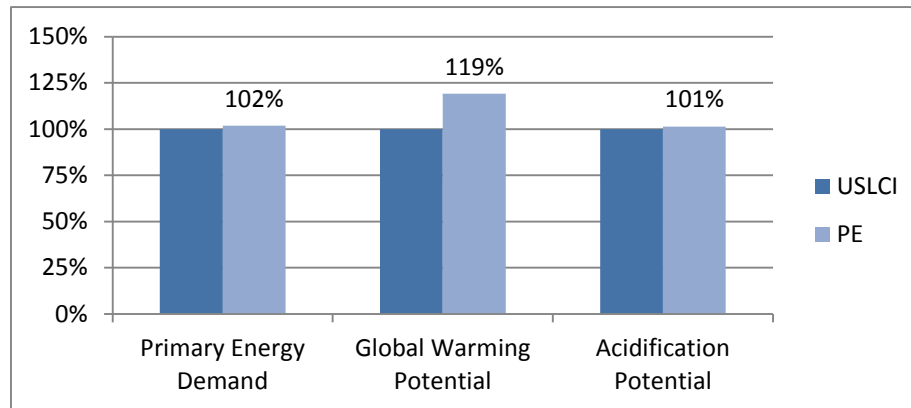
**Figure 21: 2010 Bolster Cut-off Global Warming Potential – Alternative Minus Baseline**



**Figure 22: 2010 Bolster Cut-off Acidification Potential – Alternative Minus Baseline**

## 6.4 PLASTIC DATASET COMPARISON

This study used ACC data for polypropylene resin as available in the NREL USLCI database; for other plastics PE data were used as USLCI data were not available. The primary energy demand and acidification potential of the USLCI dataset is very similar to the PE dataset “US: polypropylene granulate,” as shown in Figure 23. Though the global warming potential of the PE dataset 19% higher, using this dataset would not change whether the alternative products have a net benefit or net burden compared to the baseline; see Appendix C: Detailed Manufacturing Results for the contribution of polypropylene to global warming potential.



**Figure 23: Polypropylene Dataset Comparison**

## **7 INTERPRETATION**

### **7.1 COMPLETENESS, SENSITIVITY, AND CONSISTENCY**

#### **7.1.1 Completeness**

Completeness checks were carried out at gate-to-gate level, analyzing the completeness of process steps considered to describe the part production and the coverage of material inputs and outputs of relevance for the individual part production steps. Furthermore, the completeness was checked at cradle-to-gate level with focus on the coverage of all significant upstream data. All relevant, specific processes for the different options are considered and modeled to represent each specific situation.

#### **7.1.2 Sensitivity and Scenario Analysis**

The following scenarios were analyzed, as presented in Chapter 6:

- Adaptation to the power train, resulting in a higher fuel reduction due to lightweighting during use phase
- Cut-off approach instead of avoided burden approach for modeling scrap generation and product end-of-life

Additionally, a comparison the USLCI and PE/GaBi polypropylene datasets is provided.

A Monte Carlo analysis was performed for the key assumptions in the use phase fuel reduction calculation, and is also presented in Chapter 6.

#### **7.1.3 Consistency**

To ensure consistency only primary data of the same level of detail and the same background data from the GaBi databases are used. The material input and output (product and scrap) data provided by ACC were checked on a mass balance basis. While building up the model cross-checks concerning the plausibility of mass and energy flows were conducted.

### **7.2 LIMITATIONS, CONCLUSIONS, AND RECOMMENDATIONS**

#### **7.2.1 Limitations**

The following limitations to the study have been identified:

- Results are specific to the selected parts for this study and are not to be generalized, e.g., the average metal and plastic bolster, or to the comparison of plastic and metal parts in general.
- This study assumes the primary function of the compared parts is the same. It does not examine other potential benefits of using polymers or metal materials, such as differences in performance during crash testing, aesthetics, longevity beyond the considered 150,000 miles, etc.
- Results are specific to US boundary conditions. Different geographical regions may have different conclusions.
- This study did not collect primary energy and emissions data at the part manufacturing facilities; it used average GaBi background data for part production. It does not claim a particular potential environmental impact at a specific facility.
- The calculation of the difference in fuel consumption during use phase depends on the assumptions described in Section 4.2 and included in the Monte Carlo analysis presented in Section 6.2.



- The end-of-life stage assumes that all plastic goes to landfill and 98% of metal goes to recycling, and uses average GaBi background data to model end-of-life. It does not examine regional or local variation, where the recycling rate may differ or waste materials may be incinerated.

### 7.2.2 Conclusions and Recommendations

When comparing to the baseline product (2008 bolster):

- Applying US EPA's TRACI normalization factors demonstrates that summer smog and eutrophication potential only show minor differences compared to the 2008 bolster when compared to the other impact categories in this study.
- The lighter-than-baseline 2005 bolster and 2010 bolster perform better than the baseline 2008 bolster for global warming potential, primary energy demand, and acidification potential. The use phase is the dominant phase in the life cycle.
- The 2010 bolster is also lighter than and performs better than the 2005 bolster in all considered impact categories.
- Scenario and sensitivity analysis show that the results are conservative estimates. A greater divergence from the baseline is possible, i.e., higher savings for all lighter-than-baseline components, in the scenarios with adaptation to the power train. The cut-off approach and the mean values in the Monte Carlo analysis of the use phase savings also result in a greater divergence from the baseline.

An even greater benefit is possible if additional parts on the vehicle are also reduced in mass to an extent that allows for adaptations to the drive train or gearbox (reduction of engine displacement or elongation of gear ratio) while maintaining constant vehicle performance. These measures allow the use phase savings to be more than doubled. Since the extent of additional lightweight measures was unknown in this project, the drive train adaptation was considered as a potential scenario only. To harvest the benefits of lightweighting to their full extent, it is recommended that the sum of all mass reductions in the design process should be monitored and, whenever feasible, invested into fuel economy by adapting the drive train while maintaining constant vehicle performance. Investing lightweight measures into fuel economy will become more likely in the future since the Corporate Average Fuel Economy (CAFE) standards for model years 2012-2016 passenger cars and light trucks requires an estimated combined average mile per gallon level of 34.1 by model year 2016.

The potential benefit of plastic parts would also increase if the US adopts end-of-life regulations, such as in Europe, for re-use and recovery of vehicle parts rather than disposal to landfill, since this study assumes that all plastic goes to landfill at end-of-life based on current conditions.

Concluding, it appears reasonable to state that while the lighter products show only small differences to the 2008 bolster with regard to summer smog and eutrophication, they have the potential to lower the global warming potential, primary energy demand, and acidification potential of their metal counterpart over the full life cycle. Future conditions such as more stringent fuel economy and end-of-life regulations will likely increase this potential benefit across all impact categories. These conclusions are drawn for the specific parts examined in this study and shall not be generalized to encompass all plastic vs. metal part comparisons. Specific design options should always be assessed on a case-by-case basis as different materials or combinations of materials may render different results.

## APPENDIX A: LIFE CYCLE IMPACT ASSESSMENT CATEGORIES

Impact Category (issue)	Indicator	Description	Unit	Reference
Energy Use	Non-renewable Primary Energy Demand (PED)	A measure of the total amount of primary energy extracted from the earth. PED is expressed in energy demand from non-renewable resources (e.g. petroleum, natural gas, etc.).	MJ (net calorific value)	An operational guide to the ISO-standards (Guinée et al.) Centre for Milieukunde (CML), Leiden 2001.
Climate Change	Global Warming Potential (GWP) (100 years)	A measure of greenhouse gas emissions, such as CO <sub>2</sub> and methane. These emissions are causing an increase in the absorption of radiation emitted by the earth, increasing the natural greenhouse effect. This may in turn have adverse impacts on ecosystem health, human health and material welfare.	kg CO <sub>2</sub> equivalent	Intergovernmental Panel on Climate Change (IPCC). Climate Change 2007: The Physical Science Basis. Contribution of Working Group I to the Fourth Assessment. Report of the Intergovernmental Panel on Climate Change. 2007.
Eutrophication	Eutrophication Potential	Eutrophication covers all potential impacts of excessively high levels of macronutrients, the most important of which nitrogen (N) and phosphorus (P). Nutrient enrichment may cause an undesirable shift in species composition and elevated biomass production in both aquatic and terrestrial ecosystems. In aquatic ecosystems increased biomass production may lead to depressed oxygen levels, because of the additional consumption of oxygen in biomass decomposition.	kg N equivalent	Bare et al., TRACI: the Tool for the Reduction and Assessment of Chemical and Other Environmental Impacts JIE, MIT Press, 2002.
Acidification	Acidification Potential	A measure of emissions that cause acidifying effects to the environment. The acidification potential is a measure of a molecule's capacity to increase the hydrogen ion (H <sup>+</sup> ) concentration in the presence of water, thus decreasing the pH value. Potential effects include fish mortality, forest decline and the deterioration of building materials.	mol H <sup>+</sup> equivalent	Bare et al., TRACI: the Tool for the Reduction and Assessment of Chemical and Other Environmental Impacts JIE, MIT Press, 2002.

Impact Category (issue)	Indicator	Description	Unit	Reference
Smog	Photochemical Ozone Creation Potential (POCP)	A measure of emissions of precursors that contribute to ground level smog formation (mainly ozone O <sub>3</sub> ), produced by the reaction of VOC and carbon monoxide in the presence of nitrogen oxides under the influence of UV light. Ground level ozone may be injurious to human health and ecosystems and may also damage crops.	kg NO <sub>x</sub> equivalent	Bare et al., TRACI: the Tool for the Reduction and Assessment of Chemical and Other Environmental Impacts JIE, MIT Press, 2002.

## **APPENDIX B: CRITICAL REVIEW REPORT**

See following pages

## **Critical Review of the study "Life Cycle Assessment of Polymers in an Automotive Bolster"**

<b>Commissioned by:</b>	American Chemistry Council
<b>Performed by:</b>	PE International, Inc.
<b>Critical Review Panel:</b>	Dr. Roland Geyer, Associate Professor, Bren School, UCSB Dr. Allan Murray, President, Ecoplexus Inc., and CTO, Allied Composite Technologies LLC Dr. John Sullivan, Environmental Scientist, Sustainable Development Strategies, LLC
<b>Date:</b>	23 April, 2012
<b>Reference</b>	ISO 14040 (2006): Environmental Management - Life Cycle Assessment - Principles and Framework ISO 14044 (2006): Environmental Management - Life Cycle Assessment – Requirements and Guidelines

### **The Scope of the Critical Review**

The review panel had the task to assess whether

- the methods used to carry out the LCA are consistent with the international standards ISO 14040 and ISO 14044
- the methods used to carry out the LCA are scientifically and technically valid,
- the technological coverage of the industry is representative of the current practice,
- the data used are appropriate and reasonable in relation to the goal of the study,
- the interpretations reflect the limitations identified and the goal of the study, and
- the study report is transparent and consistent.

The review was performed according to ISO 14040 and ISO 14044 in their strictest sense as the results of the study are intended to be used for comparative assertions to be disclosed to the public.

The extent to which the unit process data are appropriate and representative, given the goal and scope of the study, was determined by a critical review of the available metadata, i.e. process descriptions, etc. Analysis and validation of the process inputs and outputs themselves was outside the scope of this review.

### **General evaluation**

The defined scope for this LCA study was found to be appropriate to achieve the defined goals. The Life Cycle Inventory model is suitable for the purpose of the study and is thus capable to

support the goal of the study. All primary and secondary data are adequate in terms of quality, and technological, geographical and temporal coverage. The data quality is found to be high. The selection of impact categories, which were limited to five, is appropriate and reasonable in relation to the goal of the study. As a result, the report is deemed to be representative and complete. The study is reported in a transparent manner. Various assumptions were addressed by sensitivity analyses of critical data and methodological choices. The interpretations of the results reflect the identified limitations of the study and are considered to be conservative.

The critical review process was open and constructive. The LCA practitioners were very cooperative and forthcoming and addressed all questions, comments, and requests of the review panel to its full satisfaction.

### **Conclusion**

The study has been carried out in compliance with ISO 14040 and ISO 14044. The critical review panel found the overall quality of its methods scientifically and technically valid and the used data appropriate and reasonable. The study report is transparent and consistent, and the interpretation of the results fully reflects the goal and the identified limitations of the study.



Roland Geyer



Allen Murray



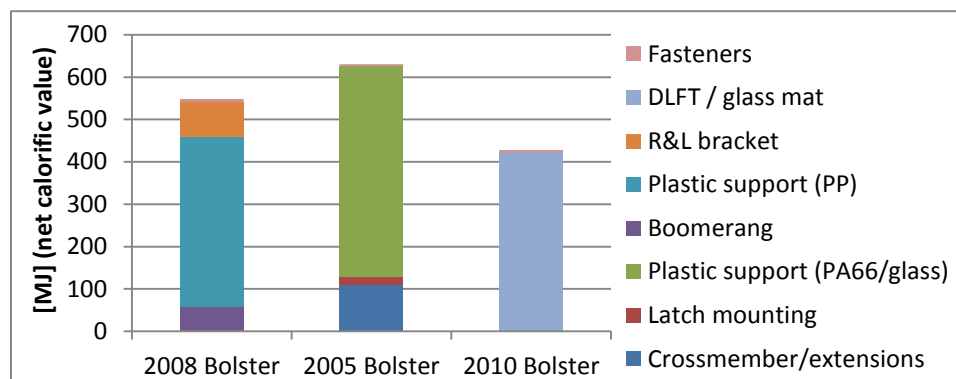
John Sullivan

## APPENDIX C: DETAILED MANUFACTURING RESULTS

This appendix shows the cradle-to-gate potential impacts from the manufacturing phase of the life cycle for each auto part, not including transportation, by component (scrap credits included) and by material or process (scrap credits shown separately).

**Table 16: Bolster Manufacturing Primary Energy Demand – by Component**

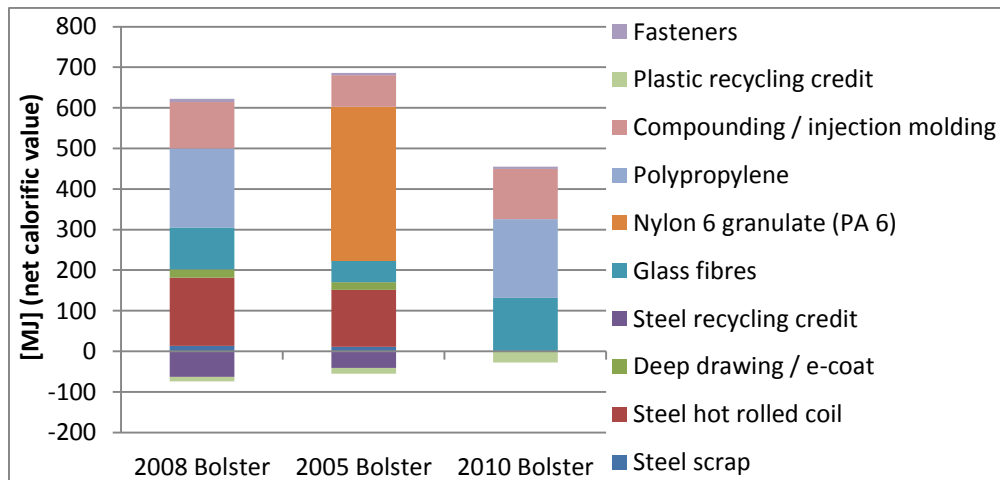
Primary Energy Demand (net calorific value) [MJ]	2008 Bolster	2005 Bolster	2010 Bolster
Crossmember/extensions		110.62	
Latch mounting		18.16	
Plastic support (PA66/glass)		496.97	
Boomerang	57.78		
Plastic support (PP)	401.54		
R&L bracket	81.27		
DLFT / glass mat			422.21
Fasteners	7.98	5.04	5.42



**Figure 24: Bolster Manufacturing Primary Energy Demand – by Component**

**Table 17: Bolster Manufacturing Primary Energy Demand – by Material/Process**

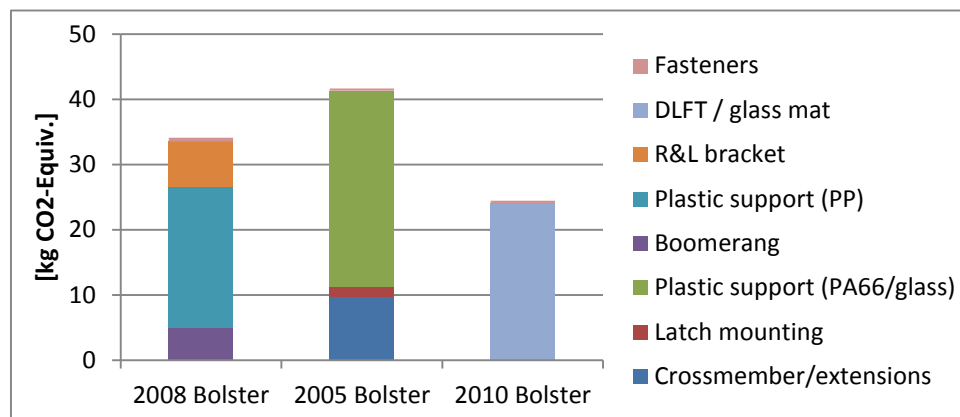
Primary Energy Demand (net calorific value) [MJ]	2008 Bolster	2005 Bolster	2010 Bolster
Steel scrap	13.58	11.36	
Steel hot rolled coil	167.53	140.21	
Deep drawing / e-coat	20.89	18.54	
Steel recycling credit	-62.95	-41.33	
Glass fibres	103.51	53.22	131.54
Nylon 6 granulate (PA 6)		379.23	
Polypropylene	194.62		193.97
Compounding / injection molding	114.41	78.43	124.04
Plastic recycling credit	-11.00	-13.92	-27.33
Fasteners	7.98	5.04	5.42



**Figure 25: Bolster Manufacturing Primary Energy Demand – by Material/Process**

**Table 18: Bolster Manufacturing Global Warming Potential – by Component**

Global Warming Potential (GWP 100 years) [kg CO2-Equiv.]	2008 Bolster	2005 Bolster	2010 Bolster
Crossmember/extensions		9.66	
Latch mounting		1.61	
Plastic support (PA66/glass)		30.07	
Boomerang	4.92		
Plastic support (PP)	21.60		
R&L bracket	7.02		
DLFT / glass mat			24.06
Fasteners	0.56	0.35	0.38

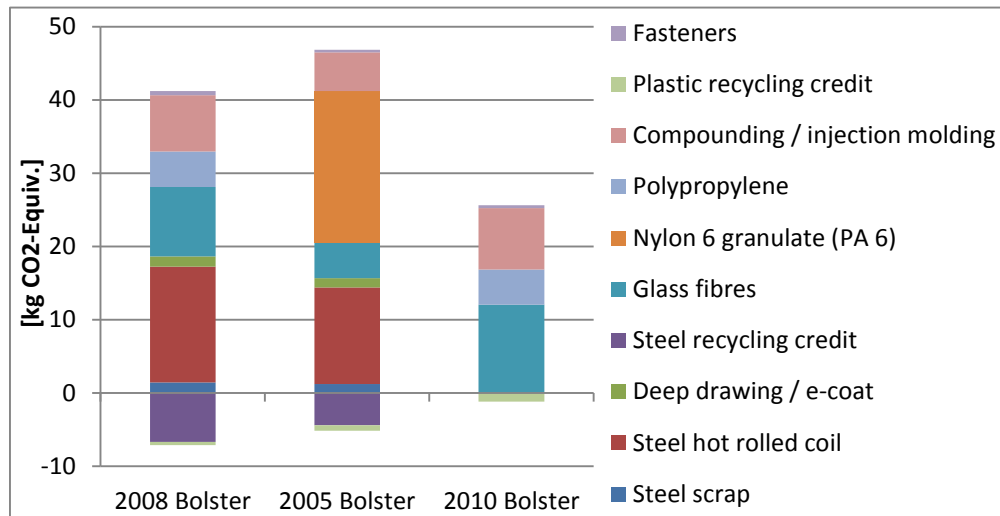


**Figure 26: Bolster Manufacturing Global Warming Potential – by Component**



**Table 19: Bolster Manufacturing Global Warming Potential – by Material/Process**

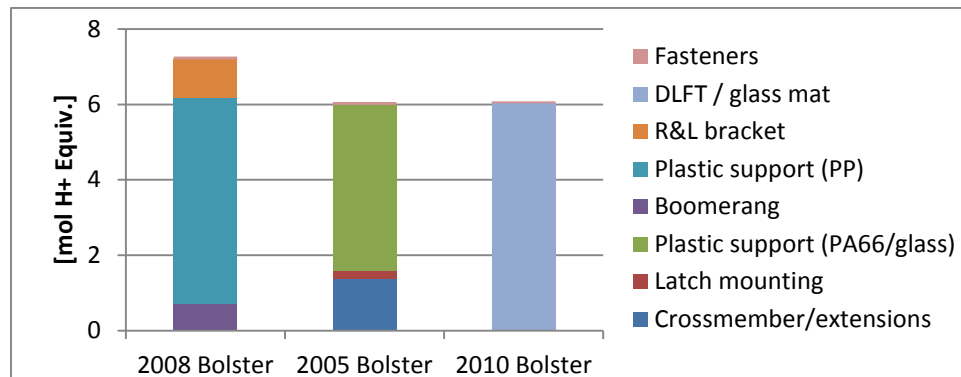
Global Warming Potential (GWP 100 years) [kg CO <sub>2</sub> -Equiv.]	2008 Bolster	2005 Bolster	2010 Bolster
Steel scrap	1.44	1.21	
Steel hot rolled coil	15.79	13.22	
Deep drawing / e-coat	1.39	1.23	
Steel recycling credit	-6.69	-4.39	
Glass fibres	9.50	4.88	12.07
Nylon 6 granulate (PA 6)		20.68	
Polypropylene	4.82		4.80
Compounding / injection molding	7.71	5.29	8.36
Plastic recycling credit	0	-0.78	-1.18
Fasteners	0.56	0.35	0.38



**Figure 27: Bolster Manufacturing Global Warming Potential – by Material/Process**

**Table 20: Bolster Manufacturing Acidification Potential – by Component**

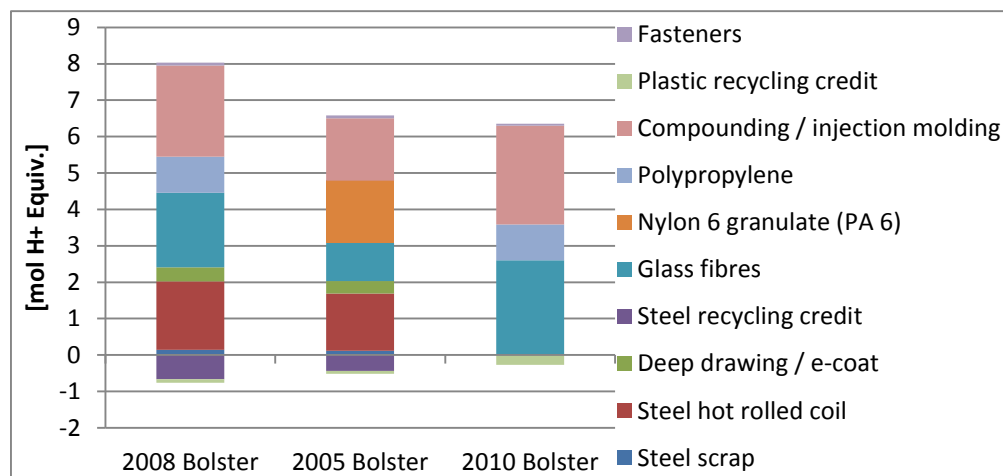
Acidification Air [mol H <sup>+</sup> Equiv.]	2008 Bolster	2005 Bolster	2010 Bolster
Crossmember/extensions		1.37	
Latch mounting		0.22	
Plastic support (PA66/glass)		4.40	
Boomerang	0.73		
Plastic support (PP)	5.44		
R&L bracket	1.02		
DLFT / glass mat			6.03
Fasteners	0.08	0.08	0.05



**Figure 28: Bolster Manufacturing Acidification Potential – by Component**

**Table 21: Bolster Manufacturing Acidification Potential – by Material/Process**

Acidification Air [mol H+ Equiv.]	2008 Bolster	2005 Bolster	2010 Bolster
Steel scrap	0.14	0.12	
Steel hot rolled coil	1.88	1.57	
Deep drawing / e-coat	0.39	0.34	
Steel recycling credit	-0.66	-0.43	
Glass fibres	2.05	1.05	2.60
Nylon 6 granulate (PA 6)		1.71	
Polypropylene	0.99		0.99
Compounding / injection molding	2.50	1.72	2.71
Plastic recycling credit	-0.10	-0.08	-0.27
Fasteners	0.08	0.08	0.05



**Figure 29: Bolster Manufacturing Acidification Potential – by Material/Process**

The plastic support for the 2008 bolster, which is 52% of the bolster by mass, contributes over 60% to each impact category. The support consists of 60% polypropylene and 40% glass fiber. The majority of the plastic support impact comes from the polypropylene material for primary energy demand, glass fibers for global warming potential, and part production (compounding and injection molding) for acidification potential.

The plastic support for the 2005 bolster contributes over 70% to all impact categories though it represents only 42% of the bolster by mass. The support consists of 70% nylon 6 and 30% glass fiber. The impact comes mostly from the nylon 6 material, though for acidification potential part production (compounding and injection molding) contributes about the same impact as nylon 6.

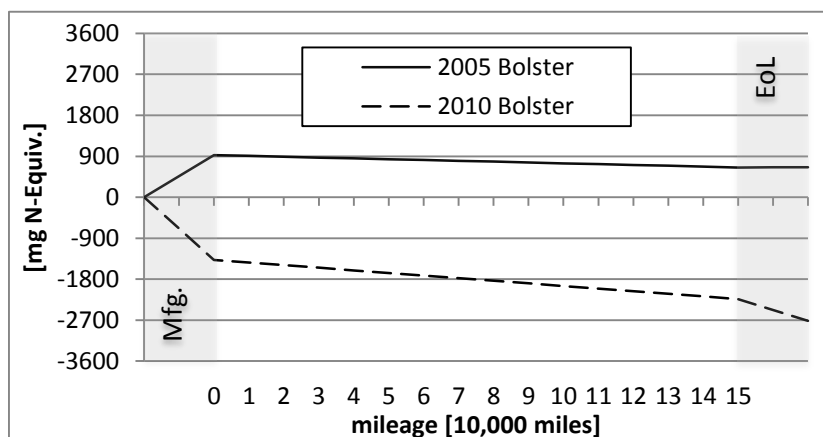
The 2010 bolster is only one component of 54% polypropylene and 46% glass fibers, plus fasteners. The majority of the plastic support impact comes from the polypropylene material for primary energy demand, glass fibers for global warming potential, and part production (compounding and injection molding) for acidification potential.

## APPENDIX D: RESULTS FOR EUTROPHICATION AND SMOG POTENTIAL

This section shows the life cycle performance for eutrophication and smog potential, and the difference from baseline (alternative product results minus baseline product results). The figures show the difference from the baseline throughout the life cycle of the vehicle and if there is a “break-even” mileage where the baseline and comparison product are equal in potential impact i.e., the impact equals zero.

**Table 22: Bolster Eutrophication Potential**

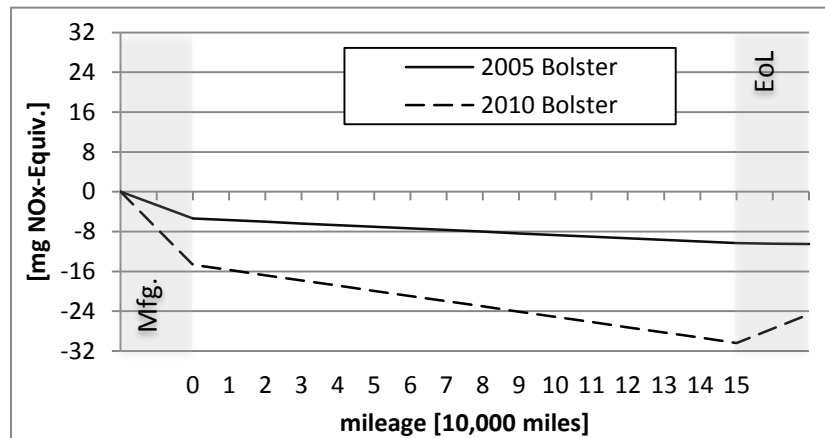
Eutrophication [mg N-Equiv.]	Absolute Results			Alternative Minus Baseline	
	2008 Bolster	2005 Bolster	2010 Bolster	2005 Bolster	2010 Bolster
Manufacturing	<b>4431.66</b>	<b>5358.16</b>	<b>3055.28</b>	<b>926.50</b>	<b>-1376.38</b>
Materials/Part Production	3874.22	5062.86	3218.79	1188.64	-655.44
Scrap Credit	557.44	295.30	-163.50	-262.14	-720.94
Use	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>-271.86</b>	<b>-860.15</b>
Fuel Production (Pre-combustion)	n/a	n/a	n/a	-271.86	-860.15
Fuel Combustion Emissions	n/a	n/a	n/a	0	0
EoL	<b>512.09</b>	<b>515.22</b>	<b>32.36</b>	<b>3.14</b>	<b>-479.72</b>
Landfill	15.69	11.18	15.57	-4.51	-0.12
Scrap Credit	496.40	504.04	16.80	7.64	-479.60
<b>Total</b>	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>658</b>	<b>-2716</b>



**Figure 30: Bolster Eutrophication Potential – Alternative Minus Baseline**

**Table 23: Bolster Smog Potential**

Smog Air [mg NOx-Equiv.]	Absolute Results			Alternative Minus Baseline	
	2008 Bolster	2005 Bolster	2010 Bolster	2005 Bolster	2010 Bolster
Manufacturing	<b>58.52</b>	<b>53.14</b>	<b>43.84</b>	<b>-5.38</b>	<b>-14.67</b>
Materials/Part Production	66.80	58.79	46.24	-8.01	-20.55
Scrap Credit	-8.28	-5.66	-2.40	2.63	5.88
Use	n/a	n/a	n/a	<b>-4.96</b>	<b>-15.69</b>
Fuel Production (Pre-combustion)	n/a	n/a	n/a	-4.96	-15.69
Fuel Combustion Emissions	n/a	n/a	n/a	0.00	0.00
EoL	<b>-5.68</b>	<b>-5.86</b>	<b>0.09</b>	<b>-0.18</b>	<b>5.78</b>
Landfill	0.30	0.21	0.30	-0.09	0
Scrap Credit	-5.98	-6.07	-0.20	-0.09	5.78
<b>Total</b>	<b>n/a</b>	<b>n/a</b>	<b>n/a</b>	<b>-10.52</b>	<b>-24.59</b>



**Figure 31: Bolster Smog Potential – Alternative Minus Baseline**

## ABOUT PE INTERNATIONAL

PE INTERNATIONAL is the premier integrated sustainability solutions provider across the globe, providing consulting, software and content that delivers measureable business impacts to the corporate and product sustainability efforts of enterprises of all sizes. Our market-leading expertise is offered through a unique portfolio of products and services that includes: Five Winds Strategic Consulting, Product Sustainability Solutions, and Corporate Sustainability Solutions.

Founded in 1991, PE INTERNATIONAL operates from 20 offices globally to assist clients in measuring, understanding and managing their sustainability footprint to create sustainable and quantifiable business value. We work with clients across all industry sectors and in all geographic regions to identify the specific challenges to optimizing their sustainability performance. Our collaborative approach supports clients in elevating their sustainability performance by integrating environmental, social and broader-based cost information into core business processes from strategy development and business planning, to capital expenditure approvals, and product development.

Our proven processes, technologies, tools and content have allowed clients to translate sustainability improvements into measureable business value by communicating sustainability improvements to all key stakeholders in easy to understand ways. The unique nature of the PE INTERNATIONAL solution portfolio allows us to deliver value across the enterprise value chain on a continuing basis. Our Five Winds Strategic Consulting services includes thought leaders and practitioners that have defined many of the key sustainability processes in general use today while our GaBi LCA software and GaBi database are the most widely used LCA tools in the world.

### PE INTERNATIONAL Solutions

- **Five Winds Strategic Consulting** – Strategic consulting that focuses on enterprise-level sustainability strategy, management systems, product innovation, carbon management and reporting.
- **Product Sustainability** – A combination of GaBi LCA Software, the leading software tool for modeling complex product systems from a Life Cycle Perspective, GaBi LCI Datasets, our regularly updated database built upon information from industry sources, scientific research, technical literature, and internal patent information, and consulting and implementation services.
- **Corporate Sustainability** – SoFi Software, a leading software platform for enterprise-wide corporate environmental management focusing on: Sustainability Information Management, Analytics, and Strategic Action Planning, and consulting and implementation services.

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